CHARDON—
HAMBDEN
E. & W. Center Road.

DIETZGEN
TRADE MARK

ENGINEERS'
FIELD BOOK
No. 400

91

EUGENE DIETZGEN CO.

DRAWING MATERIALS, MATHEMATICAL and SURVEYING INSTRUMENTS

Chicago New York San Francisco New Orleans Pittsburg Toronto

Distances from Center of Roadway for Cross-Sectioning
Roadway Offset Width Side Slopes 1 on 1.
For Single Track Embankment

H	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	H
0	8.0	8.1	8.2	8.3	8.4	8.5	8.6	8.7	8.8	8.9	0
1	9.0	9.1	9.2	9.3	9.4	9.5	9.6	9.7	9.8	9.9	1
2	10.0	10.1	10.2	10.3	10.4	10.5	10.6	10.7	10.8	10.9	2
3	11.0	11.1	11.2	11.3	11.4	11.5	11.6	11.7	11.8	11.9	3
4	12.0	12.1	12.2	12.3	12.4	12.5	12.6	12.7	12.8	12.9	4
5	13.0	13.1	13.2	13.3	13.4	13.5	13.6	13.7	13.8	13.9	5
6	14.0	14.1	14.2	14.3	14.4	14.5	14.6	14.7	14.8	14.9	6
7	15.0	15.1	15.2	15.3	15.4	15.5	15.6	15.7	15.8	15.9	7
8	16.0	16.1	16.2	16.3	16.4	16.5	16.6	16.7	16.8	16.9	8
9	17.0	17.1	17.2	17.3	17.4	17.5	17.6	17.7	17.8	17.9	9
10	18.0	18.1	18.2	18.3	18.4	18.5	18.6	18.7	18.8	18.9	10
11	19.0	19.1	19.2	19.3	19.4	19.5	19.6	19.7	19.8	19.9	11
12	20.0	20.1	20.2	20.3	20.4	20.5	20.6	20.7	20.8	20.9	12
13	21.0	21.1	21.2	21.3	21.4	21.5	21.6	21.7	21.8	21.9	13
14	22.0	22.1	22.2	22.3	22.4	22.5	22.6	22.7	22.8	22.9	14
15	23.0	23.1	23.2	23.3	23.4	23.5	23.6	23.7	23.8	23.9	15
16	24.0	24.1	24.2	24.3	24.4	24.5	24.6	24.7	24.8	24.9	16
17	25.0	25.1	25.2	25.3	25.4	25.5	25.6	25.7	25.8	25.9	17
18	26.0	26.1	26.2	26.3	26.4	26.5	26.6	26.7	26.8	26.9	18
19	27.0	27.1	27.2	27.3	27.4	27.5	27.6	27.7	27.8	27.9	19
20	28.0	28.1	28.2	28.3	28.4	28.5	28.6	28.7	28.8	28.9	20
21	29.0	29.1	29.2	29.3	29.4	29.5	29.6	29.7	29.8	29.9	21
22	30.0	30.1	30.2	30.3	30.4	30.5	30.6	30.7	30.8	30.9	22
23	31.0	31.1	31.2	31.3	31.4	31.5	31.6	31.7	31.8	31.9	23
24	32.0	32.1	32.2	32.3	32.4	32.5	32.6	32.7	32.8	32.9	24
25	33.0	33.1	33.2	33.3	33.4	33.5	33.6	33.7	33.8	33.9	25
26	34.0	34.1	34.2	34.3	34.4	34.5	34.6	34.7	34.8	34.9	26
27	35.0	35.1	35.2	35.3	35.4	35.5	35.6	35.7	35.8	35.9	27
28	36.0	36.1	36.2	36.3	36.4	36.5	36.6	36.7	36.8	36.9	28
29	37.0	37.1	37.2	37.3	37.4	37.5	37.6	37.7	37.8	37.9	29
30	38.0	38.1	38.2	38.3	38.4	38.5	38.6	38.7	38.8	38.9	30
31	39.0	39.1	39.2	39.3	39.4	39.5	39.6	39.7	39.8	39.9	31
32	40.0	40.1	40.2	40.3	40.4	40.5	40.6	40.7	40.8	40.9	32
33	41.0	41.1	41.2	41.3	41.4	41.5	41.6	41.7	41.8	41.9	33
34	42.0	42.1	42.2	42.3	42.4	42.5	42.6	42.7	42.8	42.9	34
35	43.0	43.1	43.2	43.3	43.4	43.5	43.6	43.7	43.8	43.9	35
36	44.0	44.1	44.2	44.3	44.4	44.5	44.6	44.7	44.8	44.9	36
37	45.0	45.1	45.2	45.3	45.4	45.5	45.6	45.7	45.8	45.9	37
38	46.0	46.1	46.2	46.3	46.4	46.5	46.6	46.7	46.8	46.9	38
39	47.0	47.1	47.2	47.3	47.4	47.5	47.6	47.7	47.8	47.9	39
40	48.0	48.1	48.2	48.3	48.4	48.5	48.6	48.7	48.8	48.9	40

Example—If point is 22.6 ft. above grade, how far should it be from center line to be a slope stake point? Ans. from Table 30.6. For same slopes but other widths of roadbed, correct above figures by one-half difference in width of roadbed; thus in example above, for 20 ft. roadbed distance will be 30.6+(20—16)÷2 or 2 ft. added to 30.6 =32.6. For slopes of 1 on 1½ see inside of back cover.

Chardon Hamblen E & W

Center Rd

Lewis Rd

Owen Rd

WOODIN
Hamlogen Center Rd. - No. 25
Sections - A B C & D
Align. - pg. 4 - 20 & pg 39 to 48
X-Sections - pg. 22 - 37, 44 - 51

Lewis Road = Cutts Rd #72

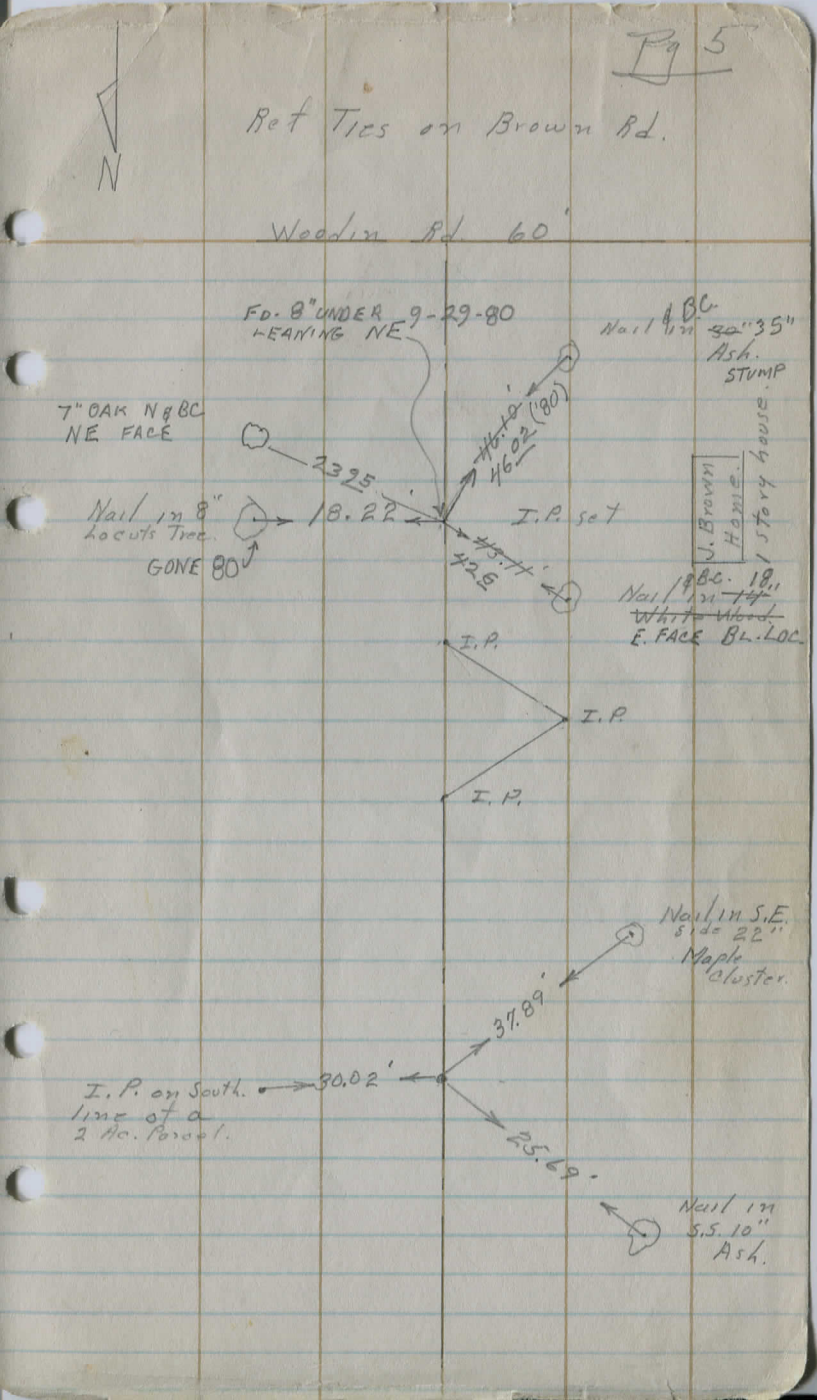
pg - 68-69

1966
Pg 77

SUMNER
~~Owen~~ Road T.N. 67

pg - 72-74

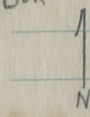
Pearl Rd see loose sheets?
BROWN TR 71 " WHY NOT ENTERED?


N
Ref Ties on Brown Rd.
Weedin Rd 60'
FD. 8" UNDER LEANING NE 9-29-80
Nail & BC in 35" Ash. STUMP
7" OAK N & BC NE FACE
23.25'
Nail in 8" Locusts Tree. GONE 80
18.22'
I.P. set
46.40' (80)
46.02'
43.7'
42.6'
J. Brown Home. 1 Story House.
Nail & BC in White Wood E. FACE BL. LOC. 18.1'
I.P.
I.P.
I.P.
Nail in S.E. side 22" Maple cluster.
37.89'
I.P. on South line of a 2 Ac. Parcel.
30.02'
25.69'
Nail in S.S. 10" Ash.

R.E. HERSHBERGER
G.L. KOVACH
D. LEWIS
N. BURT

BROWN RD.
√ SURVEY
EDM

19 APR. 1982
66°, P.C., WINDY
28.45" BAR.
CORRECTION +13



HI 4.67
P.1

792.49
.50
.53
.51

28.5" BAR
70°F.

H.I. 5.16

P.1

273°13'58" INV.

86°47'57" DIR.

101°17'26"
101°17'30"
101°17'27"
101°17'27"
AVE

T.P H.I. 5.43

203°33'20"

8.5 40'01" DIR.
274 21 59 INV.

142.06
142.02
141.97
142.00
141.96
142.02

1504.83
.84
.85
.87

164°50'22½"

P.I. 5.42

DIR. 91°05'08"
INV. 268°56'59"

P.O.T.

H.I. 6.26

DIR 89.02.24
INV 270°59'40"

N 4°45'08.75" E
4981.711'

347780'
82
83
84

179°42'43"

88°57'52"

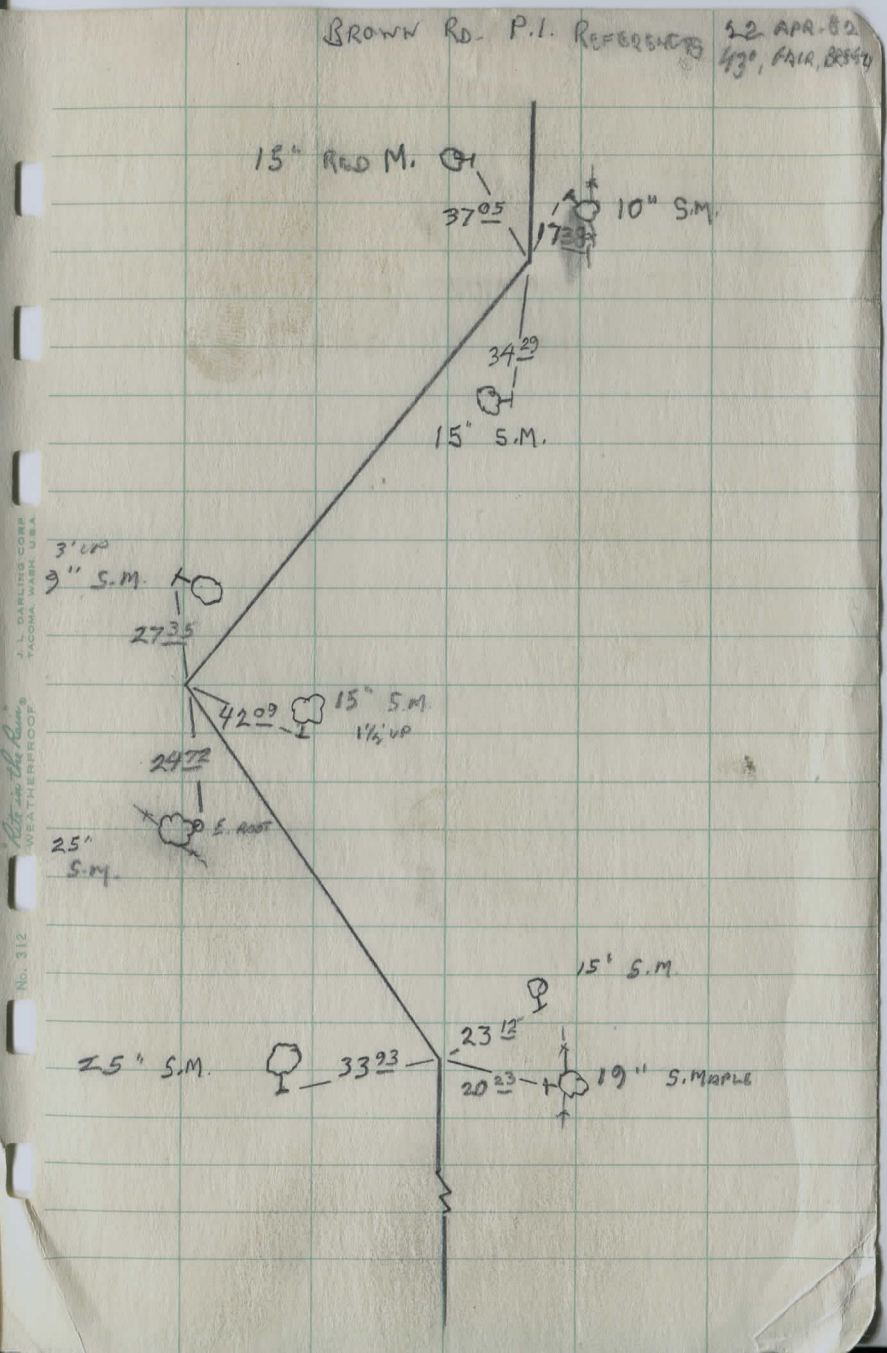
30 44 51¼

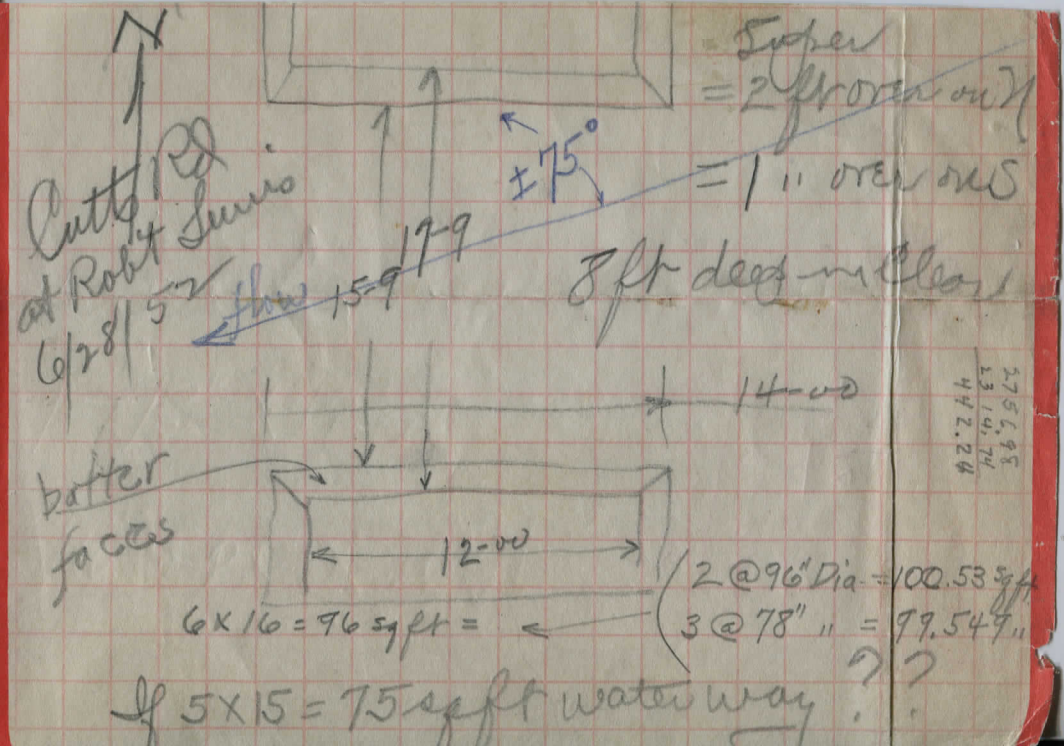
HAMBDEN CTR. RD.
WOODIN

H.I. 6.5 P.I.

℄ CH 25
E CUTTS

J.L. DARLING CORP.
TACOMA WASH. U.S.A.
"Rite in the Rain"
WEATHERPROOF
No. 312


BROWN RD. P.I. REFERENCES
22 APR. 82
43°, FAIR, BREEZY
15" RED M.
37 05
10" S.M.
17 39
34 29
15" S.M.
3' UP
9" S.M.
27 35
42 09
15" S.M.
1½' UP
24 72
E. ROOT
25" S.M.
15" S.M.
23 13
25" S.M.
33 23
20 23
19" S.M. MAPLE


Super
= 2 frozen on 7
= 1 " over ons
Cutt 28
at Robt Lewis
6/28/52
flow
15-9
17-9
±75°
8 ft deep in Clear
14-00
batter
faces
12-00
6 x 16 = 96 sq ft =
2 @ 96" Dia = 100.53 sq ft
3 @ 78" " = 99.549 "
?
?
If 5 x 15 = 75 sq ft water way
2756.98
3 14.74
442.24

33 + 98.1 ft Innocence – Rocky Line
+4 22.5 " spike on Tangent

357 Vol 2

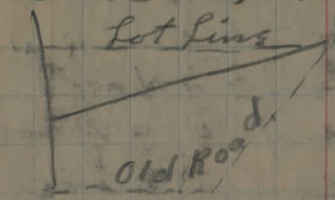
Book B, Page 423, Road Records

C.	21
C	474
D	386
D	419
A	456
B.	380

Book A. P. 380 Dec. 12, 1828
Survey of a road beginning in the center of the State Road leading from Paincville to Warren on the East & West centre line of Twp. of Hambden, thence running S. 88° W on said ℄ 2 miles 14.90 to the W. line of Hambden

Book B, P. 427 Jan. 3, 1830
beginning on the road leading from Chardon to Paincville, thence running 88° E 16.50 ch on the line between John King and Benj. Rider Jun.;
thence N. 61° E. 15.57 ch
thence N. 55° E 14 ch.
thence N. 80° E 8.48 ch.
thence N. 86° 40' E. 6.16 ch.
thence N 81° 15' E. 8.80 ch.
" S. 74° E. 12.09 ch.
" N 88° E 25.92 ch.
" N 62° 45' E. 6.25 ch.
to the road running from the centre of Hambden to the W. line of said Twp.

Book C, P. 21 May 28, 1832



bg. in c. of road from Chardon to Paincsville, from which Benj. Rider Junr. well pump bears N 42 3/4° E. 86 links
Thence N 82° E 40 chains to centre of road leading from Chardon to Paincsville

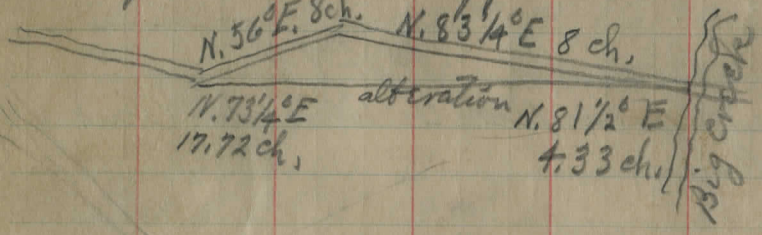
Book C, P. 474
Chard-Mentor Road to Chardon Paincsville Road.

Book D, P. 386 June 15, 1861
bg. on E. line of Chardon Twp at a stone 4.19 ch, N. of N.E. Cor. of lot 34
- S. 88° W. 25.92 ch. to a stone
- N. 74° W - 5.27 ch. to a stone
- S. 81 1/4° W 8.80 ch. to a stone
- S 86° 40' W. 6.16 ch to a stone
- S 80° W 8.48 ch to a stone
- S 55° W 7.05 ch to a stone
- S. 72 1/4° W 36.75 ch. to center of Chard-Paincsville Road.

Book D, P. 419 Sep 15, 1866

beginning at a stone sunk at the first angle east of the Hardenville road.

Thence on the same course N. 73 1/4° E. 17.72 ch to a stake - N. 81 1/2° E. 4.33 ch. to a stone sunk at the first angle west of Big Creek, The Road from thence being the same as the last mentioned course as shown by the plat hereto appended.



36.75 ch.
66
22050
22050
2425.50 ft.

17.72 ch.
66
10632
10632
1169.52 ft.

4.33
66
2598
2598
285.78

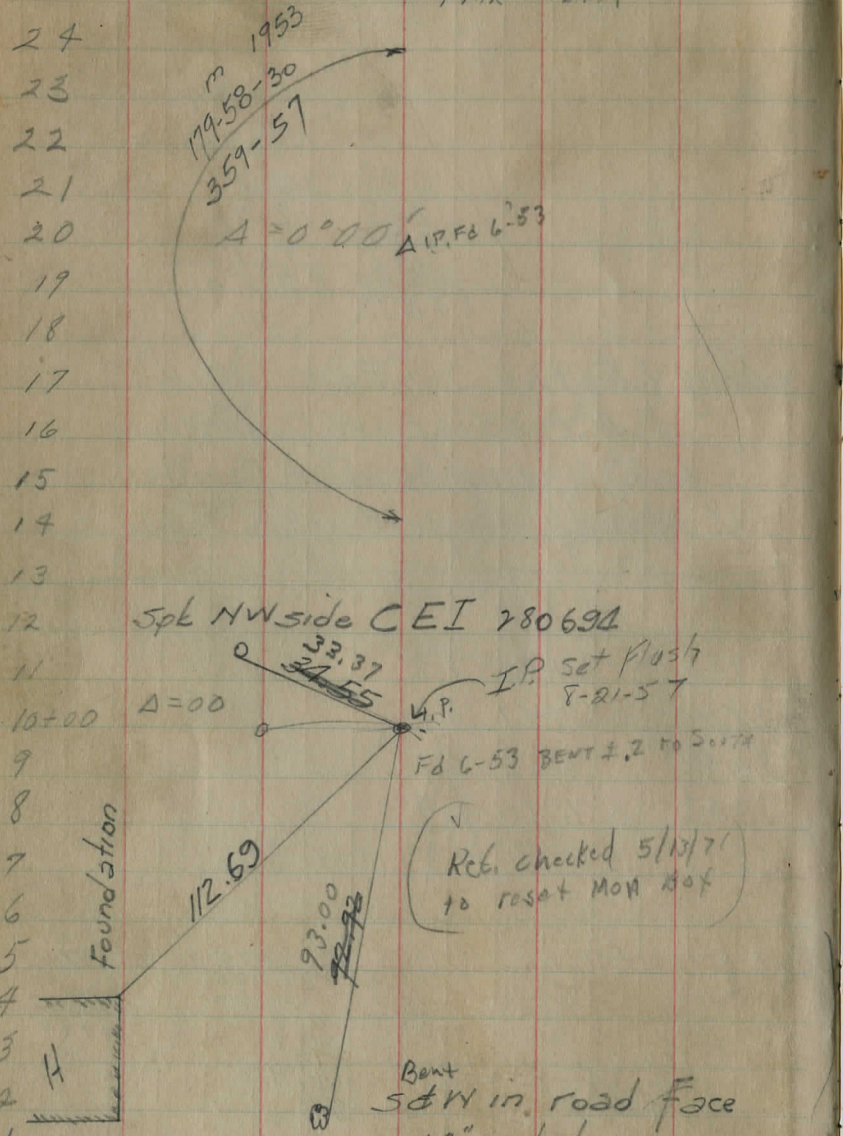
36.75 36.75
7.05 17.72
8.48 4.33
6.16
58.44 58.80

Aug-25, 1925 Fair - arid.
E. A. Fiedler, W. C. Marks,
L. T. Reynolds, E. A. Fiedler
Locating Angle Points.

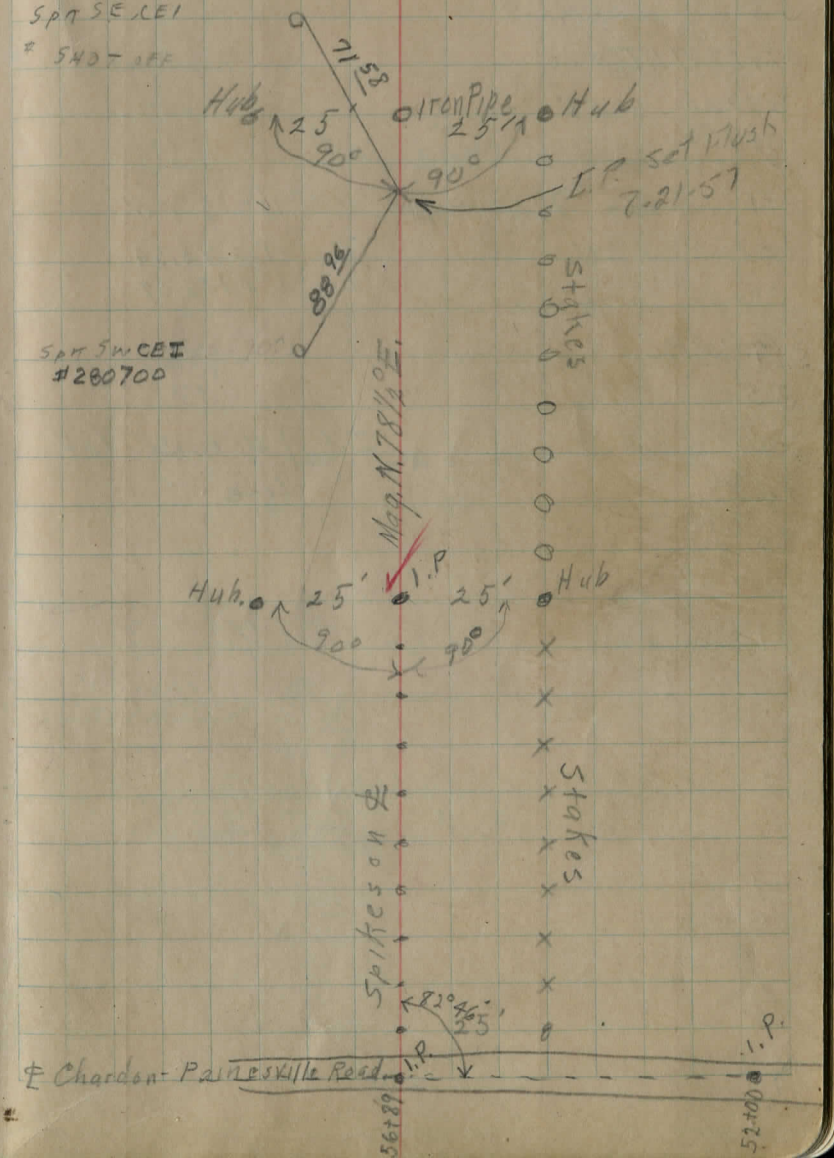
900'	1.78	1.8
1960'	3.87	3.9
3045	6.02	6.1
3443	6.80	6.9
3638	7.19	7.3 Correction

3638 7.1900 1976 .1976 .1976 .1976
3638 3443 30 45 1960 9.
35520 5928 9880 0000
32742 7904 7904 11856 1.7784
27780 7904 12784
25466 5928 5928 1976
2314 6803368 6.01692 0 38 29 60
3.89

Aug. 21, 1957 Confirm Adams
Fair-Warm



Aug. 26, 1925
Fair, Warm.
Marks
Reynolds
Parks.



40

39

38

72.53
37+27.47 P.T. 4°40'

37+00 3°59'

36+50

36+34.84 2°44' 9-18 '53

P.I. Δ = 9°20' Right. D = 5°00'

36 1°29' T = 93.54

35+50 0°14' L = 186.67

35+40 P.C.

35 '53

34+50 Δ I.P. Fd 0.15' N of line

34

33

32

31

30 Δ = 0°00'

29

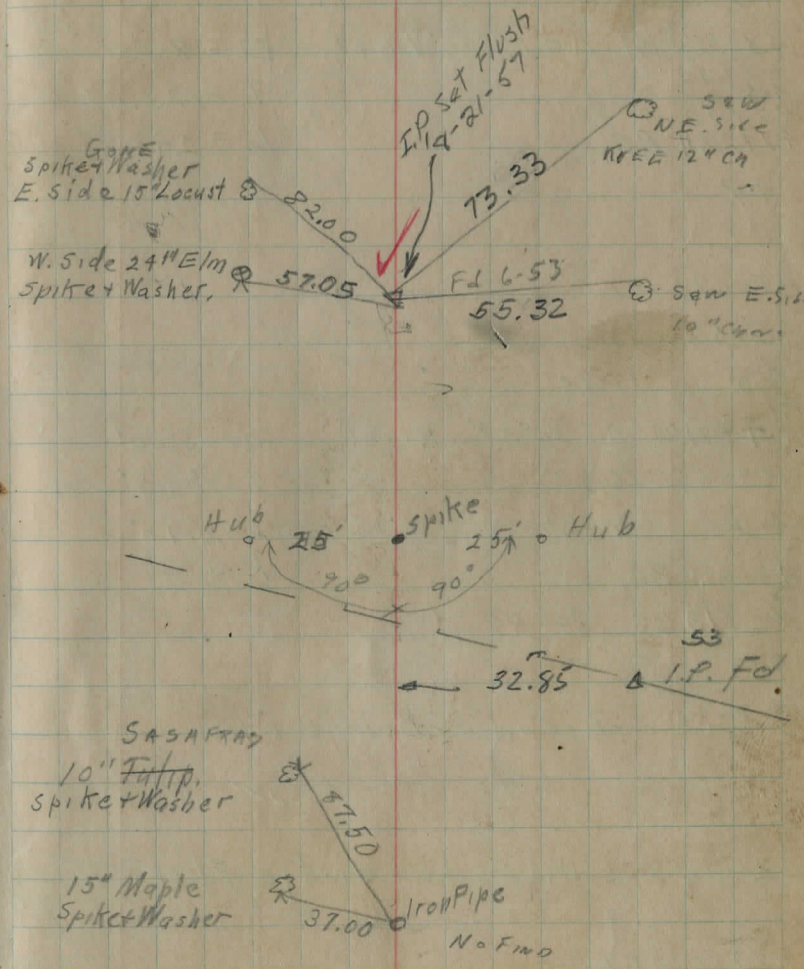
28

27

26

25

Aug. 27, 1925 Marks ½ day
Fair - Temperate Parks 1 day
Reynolds 1 day



49+72.86 P.T. 9°45'
49+50 8°50'
49 6°50'

distance from tan. to curve
0.36
3.70
10.20
3.50
0.30

48+52.15 P.I. -Δ = 19°30' Left D = 8°00'
48+50 4°50'
48 2°50'
47+50 0°50'
47+29.11 P.C. T = 123.07
L = 243.75
R = 716.20

47

46

45+69.1 P.T. 15°05'
45+50 13°39'
45 9°54'

distance from Tan. to curve
0.48
6.25
8.78
1.33

P.I. 44+71.2+ Δ = 30°09' Right D = 15°00'
44+50 6°09' T = 102.9'
44 2°24' L = 201.0'
R = 381.97
43+68.1 P.C.

43+13.26 ℄ Road North

43

42+50.3 E. end of Bridge Floor

42+12.35 W. End of Bridge Floor

42+00.55 P.T. 1°40'
42 1°40'

P.I. 41+17.24 Δ = 3°20' Left D = 2°00'
41 0°40' T = 83.36
P.C. 40+33.88 0°00' L = 166.67

6

Set W. Root 19" ASH
86.02
S&W W CEI = 277788
33.86
DRILL HOLE IN
S&W E CEI 275120
21.70
I.P. Fd 4.90 SS
40.16
Spike + Washer 24" Maple

T.L. comes off edge of pavem't should be set after ditches & berms are taken care of

Spike + Washer N.W. Root 18" Elm
18.65
I.P. set 6-10-55
19.25
Spike + Washer N.E. side 12" Cherry
S&W Rd Fnce 36" Elm
S&W SE 7" Ash
50.61
36.55
I Pin set in Pavem't 8-10-55
T.H. 76
60.73
I.P. Fd 4.30 SS
S&W SW 22" Walnut
7.7'
6.3'
6.9
7.1
S&W Sly Elm 14" TREE CLUMP
S&W NE CEI 550075
82.38
55.02
I.P. Set Flush 8-21-55
53.02
S&W W. SIDE 8" SYCAMORE
Fd 4.63
80.39
S&W SE 14" WALNUT

67

66+80.33 P.T. 16°48'

66+50 13°46'

66 8°46'

65+98.83 P.I. Δ = 33°36' Left

65+50 3°46'

65+12.33 P.C.

64

63

62

61

60

59+28.50 P.O.T. 0900' I. Pipe Fd 5-3-55 BENT & Straightened

59

58

57

56

55

54

53

52

51

50

distance from tan. to curve 7.60

11.26

From Pin on Twp. Line

D = 20°00'

T = 86.50

L = 168.00

R = 286.48

2.07 distance from tan. to curve

NOTE: See pg 20 for Const. ℄ Sta 59+28.5 to 78+0

59+28.50

42 50.3

= 16 78.2

55 Sta

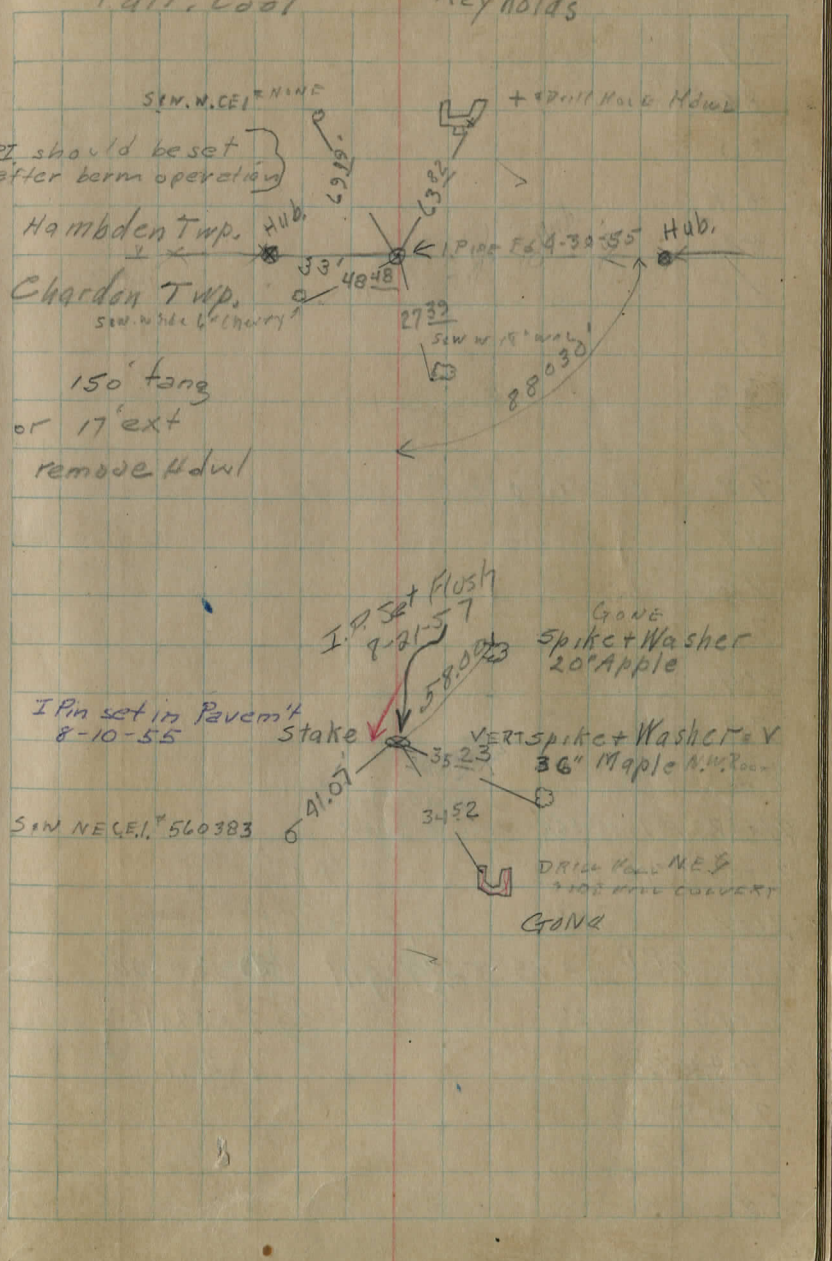
Aug. 28, 1925

Fair, Cool

Marks

Reynolds

7



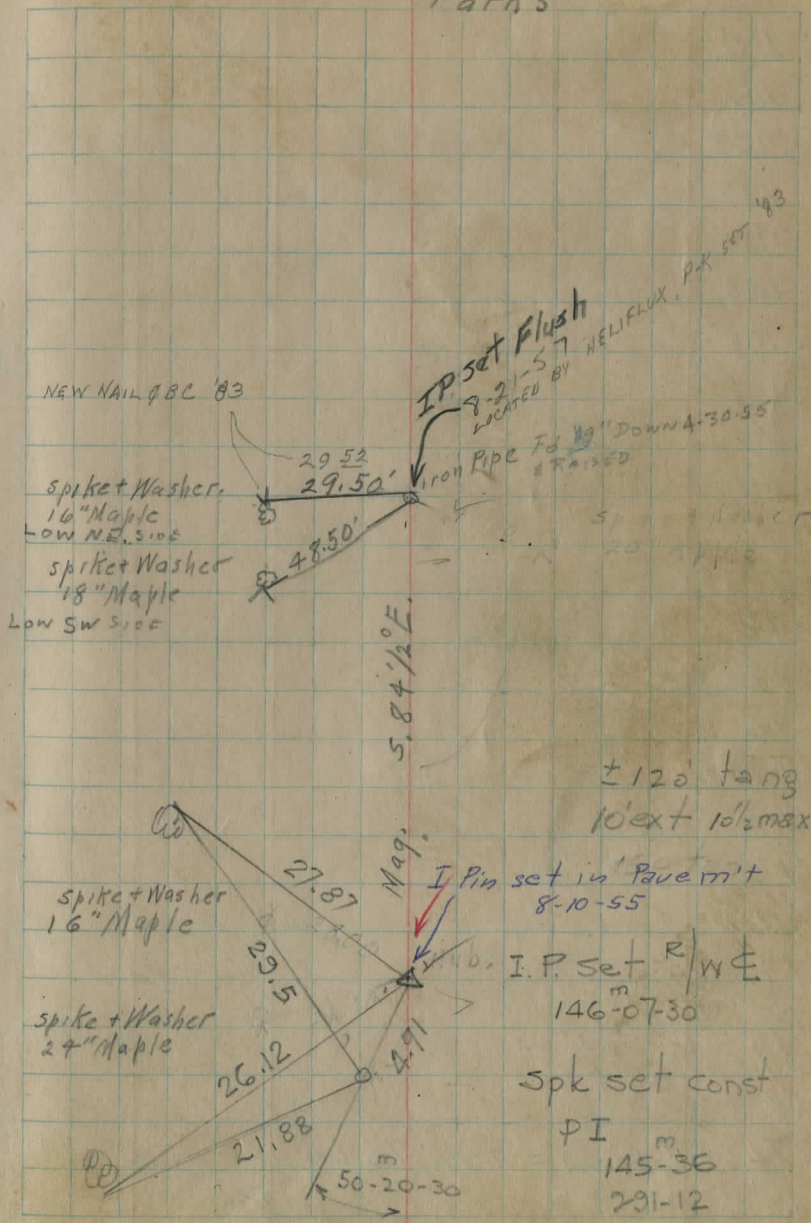
87
86
85
84
83
82
81
80
79
78 P.O.T. 0°00'
77
76
75
74
73
72
71+57.7 P.T. 16°56½'
71+25 12° 02'
71+00 8°17'
71+62.36 P.I. Δ = 33°52½' Right
70+75 4°32'
70+44.80 P.C.
70
69
68

distance from ten. to curve
2.80
8.72
2.39

D = 30°00'
T = 58.16
L = 112.9
R = 190.98

Aug. 29, 1925
Fair, Warm

Marks
Reynolds
Parks

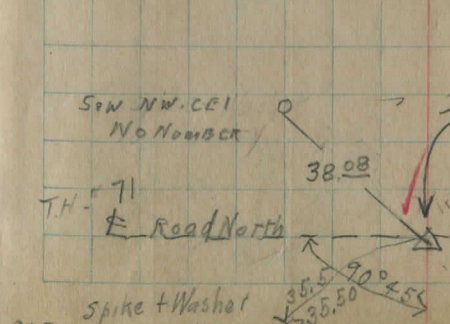


110
109
108
107
106
105
104
103
102
101
100
99
98
97
96
95
94
93
92
91
90
89
88
87+64.8 P.I. Δ = 0°17' Left

Aug. 31, 1925
Fair,

Marks
Reynolds
Parks

Stopped, Aug. 29, 1925



38.08

Fieldw. x Dirty 4/27-1926 (Temp. 22°; 5:30 Cass

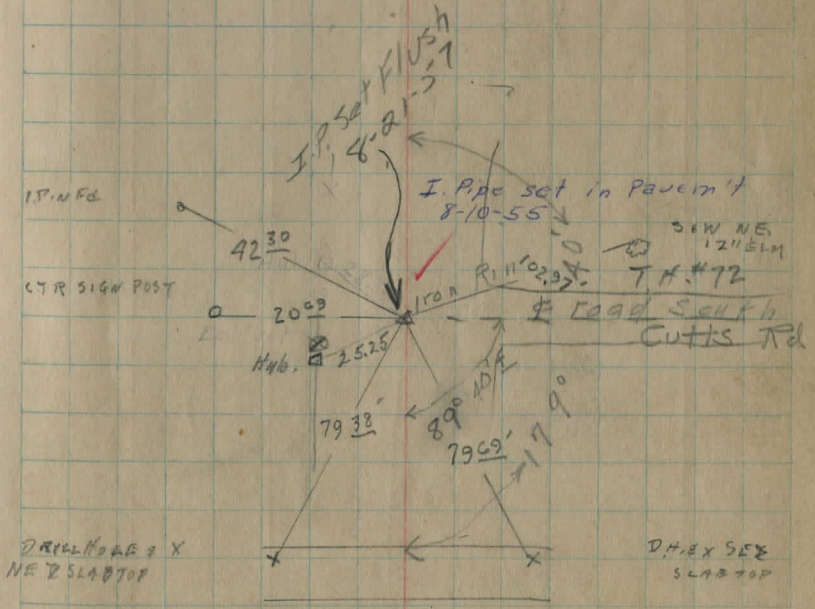
From 119+72 East.

+98.1
133
132
131
130
129
128
127
126
125
124
123
122
121
120
119+72,0 P.I. = Δ 0°-20' R. I. PIPE FL. 5-55
119
118
117
116
115
114
113
112
111

Transit note continued after x sec. Sta. 119+72

39

P.I. Iron pipe set
Prop. Line



17+08 — 14.4 — 8.8 — 8" V. P. Culvert, No. th. W.s

15+16 — 18.5

13+45

12+63 — 16.7

10+11 — 14.5

9+35 ≈

9+16 Funstein — H — 65'±

8+84

8+60 — 18.3

7+45 — 18.3

7+44 — 14.7

4+93 — 16'

2+41 Tel. — 16.7

TOPO WOODIN RD

2+00

21' — 1+70 20" Apple

1+00

0+63 — 17.4

25.5 — 0+33 El. Light

Tel. — 16.6 — 16.8'

0+14

30+71 + 11.8
30+20 30+40 Drive
H
30+12
90'
16" Maple 30+25 24.8

28+47

29+10 6.7 11.7 9" V.P. Culvert, N.of N.S.

27+98 + 13.5

27+10

16.0 26+79

21.3 26+45

26+12 26.3 26+40

15' 26+15 20" Maple

25+60 12" Maple 25

25+45 12" Maple 24.3

25+42 + 18.7

25+35

25+00

21.9 8" Elm 24+66

20' 3-6" Ash 24+53

19.7 8" Apple 24+38

23+22

22+92 + 16.7

20+35 + 17.5

13 trees

17+84 + 17.9

18.5 39+98 20" Maple

17.3 39+52 20" Maple

12.3 39+05 28" Elm

12.4 18" Maple 38+90

13.4 38+85 42" Ash

37+66

37+64 + 41.3

11.7 37+28 30" Locust

36+95

B

36+52

10' 35+83 20" Ash

12" Apple 35+67 13'

Woods

Old Meadow

12.5' 35+54 24" Maple

34+71

H

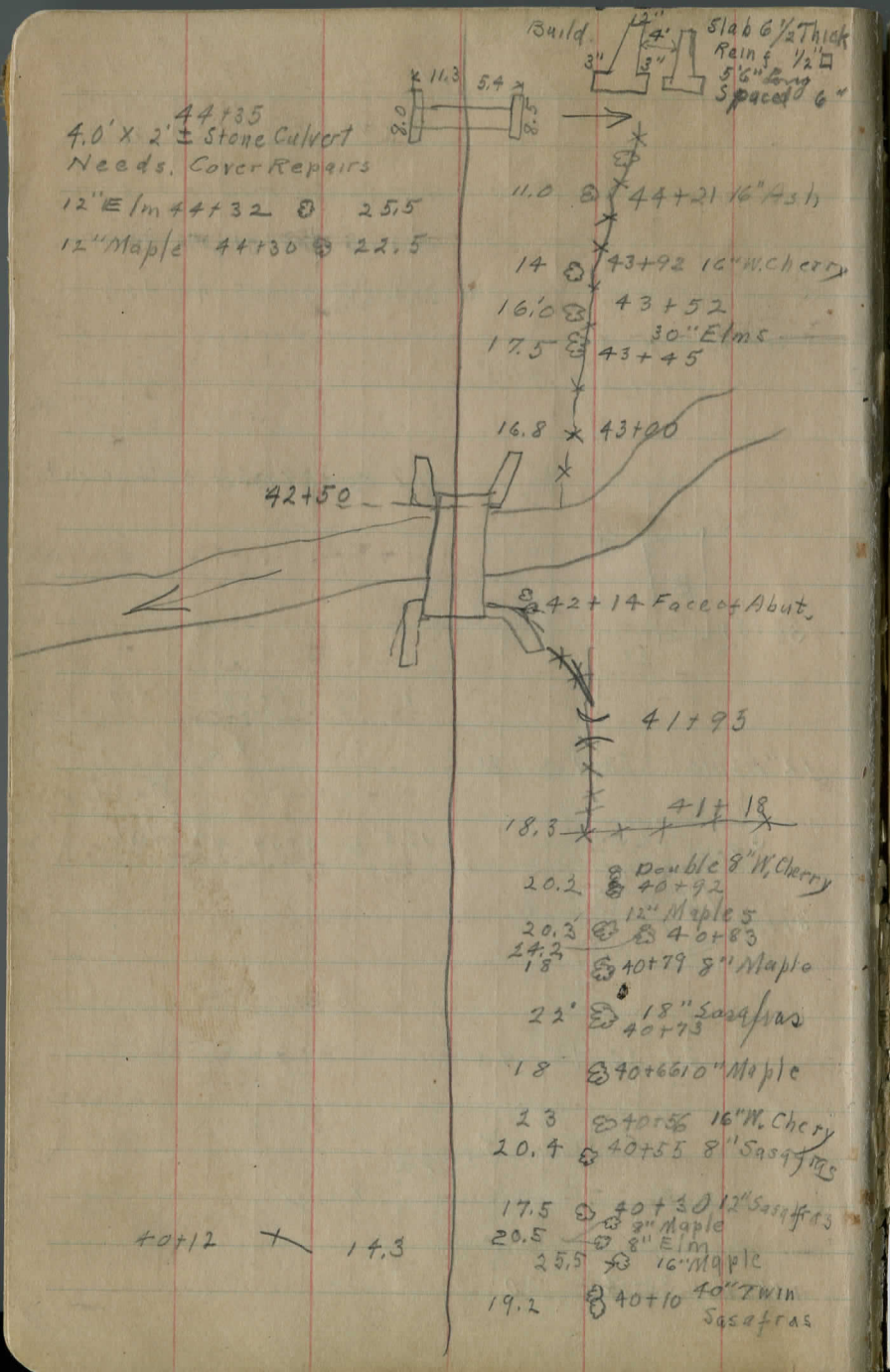
34+31 100'

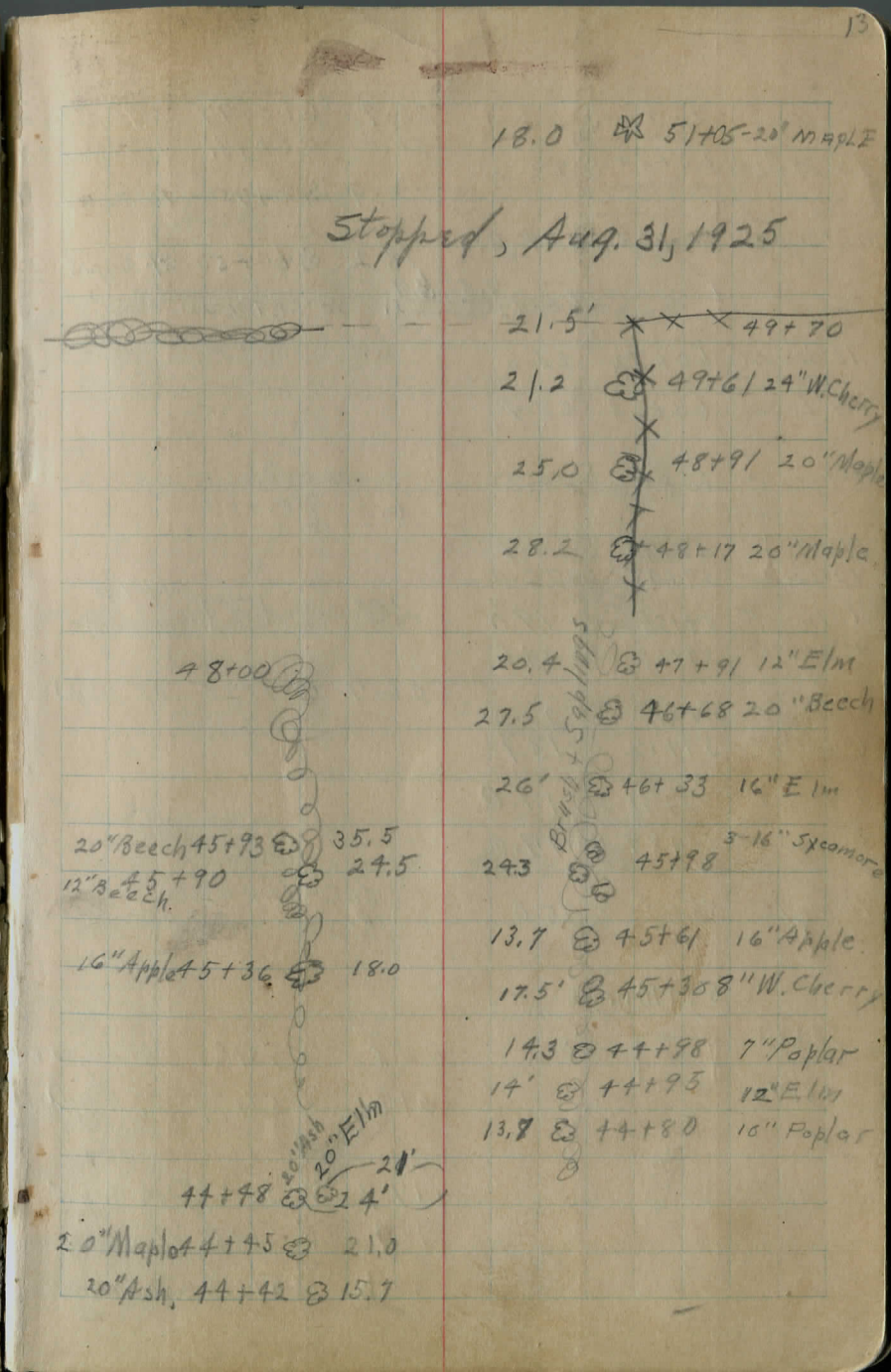
34+25

34+20 + 19.3

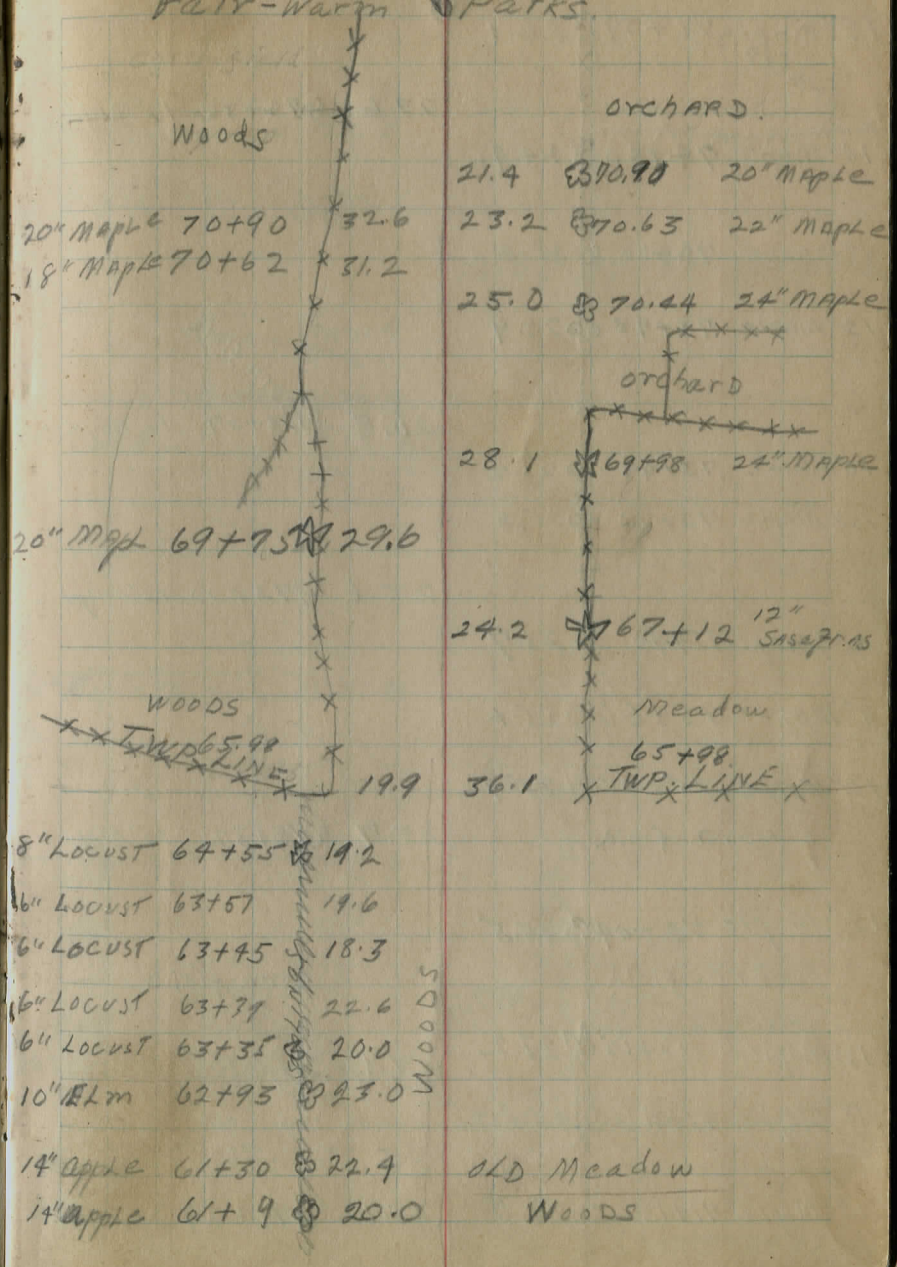
32+74

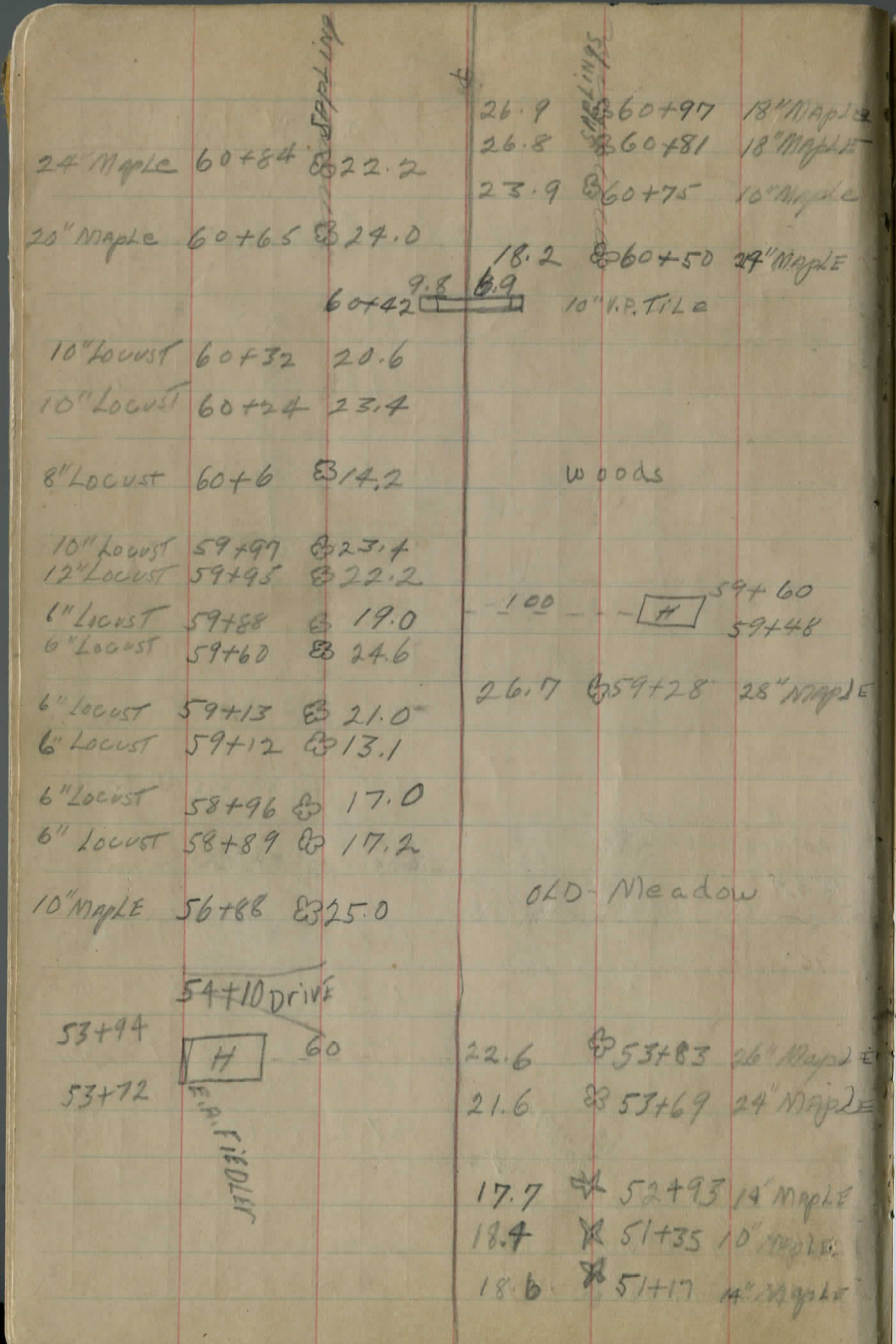
10" Tulip 30+84 20'

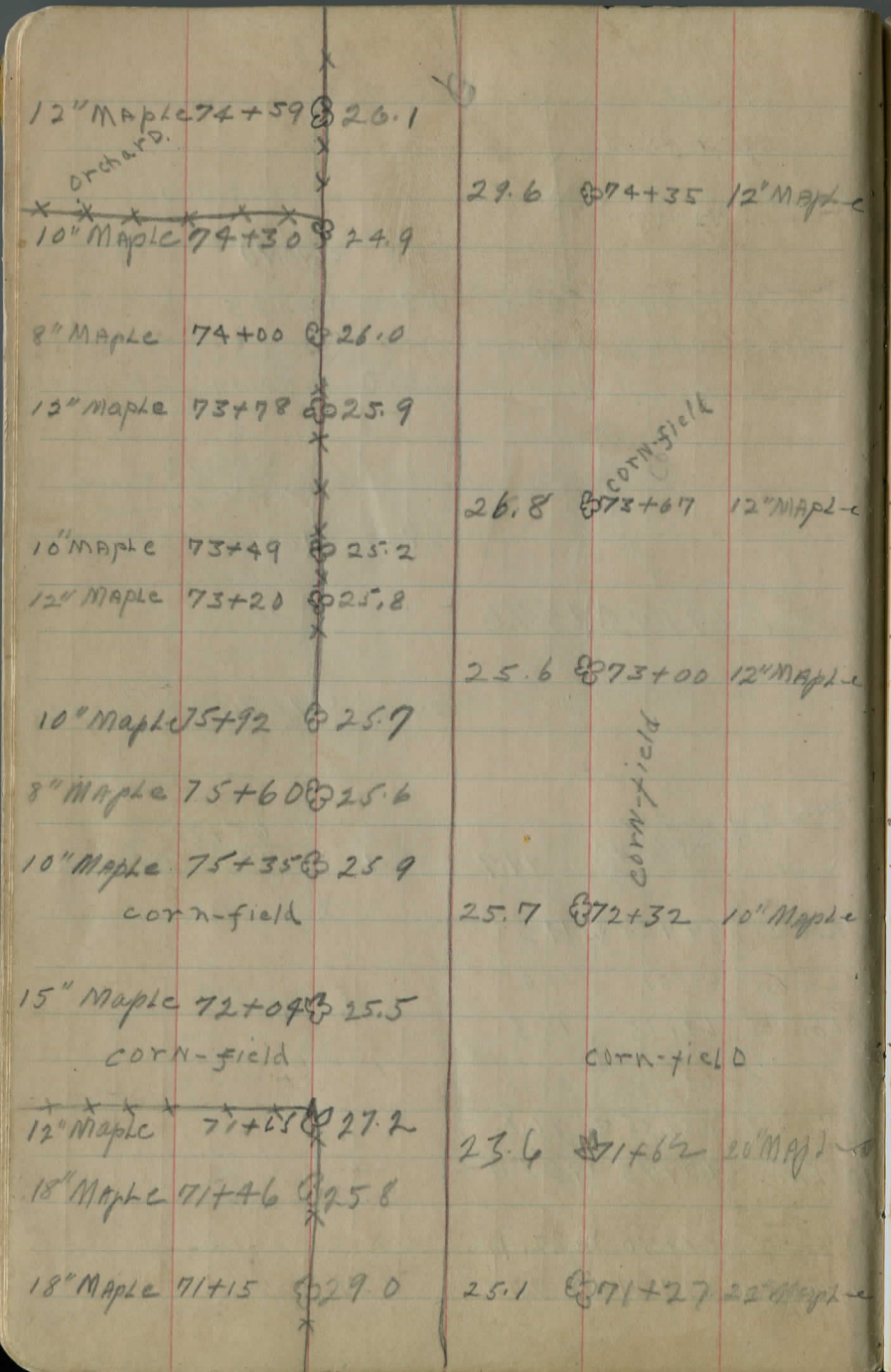

Build
4"
4'
3"
3"
Slab 6½ Thick
Reinf
½" □
5'6" Long
Spaced 6"
44+35
4.0' X 2' ± Stone Culvert
Needs Cover Repairs
12" Elm 44+32 25.5
12" Maple 44+30 22.5
11.3
5.4
2.0
2.5
11.0 44+21 16" Ash
14 43+92 16" W. Cherry
16.0 43+52
30" Elms
17.5 43+45
16.8 43+00
42+50
42+14 Face of Abut.
41+93
41+18
18.3
20.2 Double 8" W. Cherry 40+92
20.2 12" Maple 5 40+83
14.2
18 40+79 8" Maple
22' 18" Sassafras 40+73
18 40+66 10" Maple
23 40+56 16" W. Cherry
20.4 40+55 8" Sassafras
17.5 40+30 12" Sassafras
20.5 3" Maple
8" Elm
25.5 16" Maple
19.2 40+10 40" Twin Sassafras
40+12
14.3

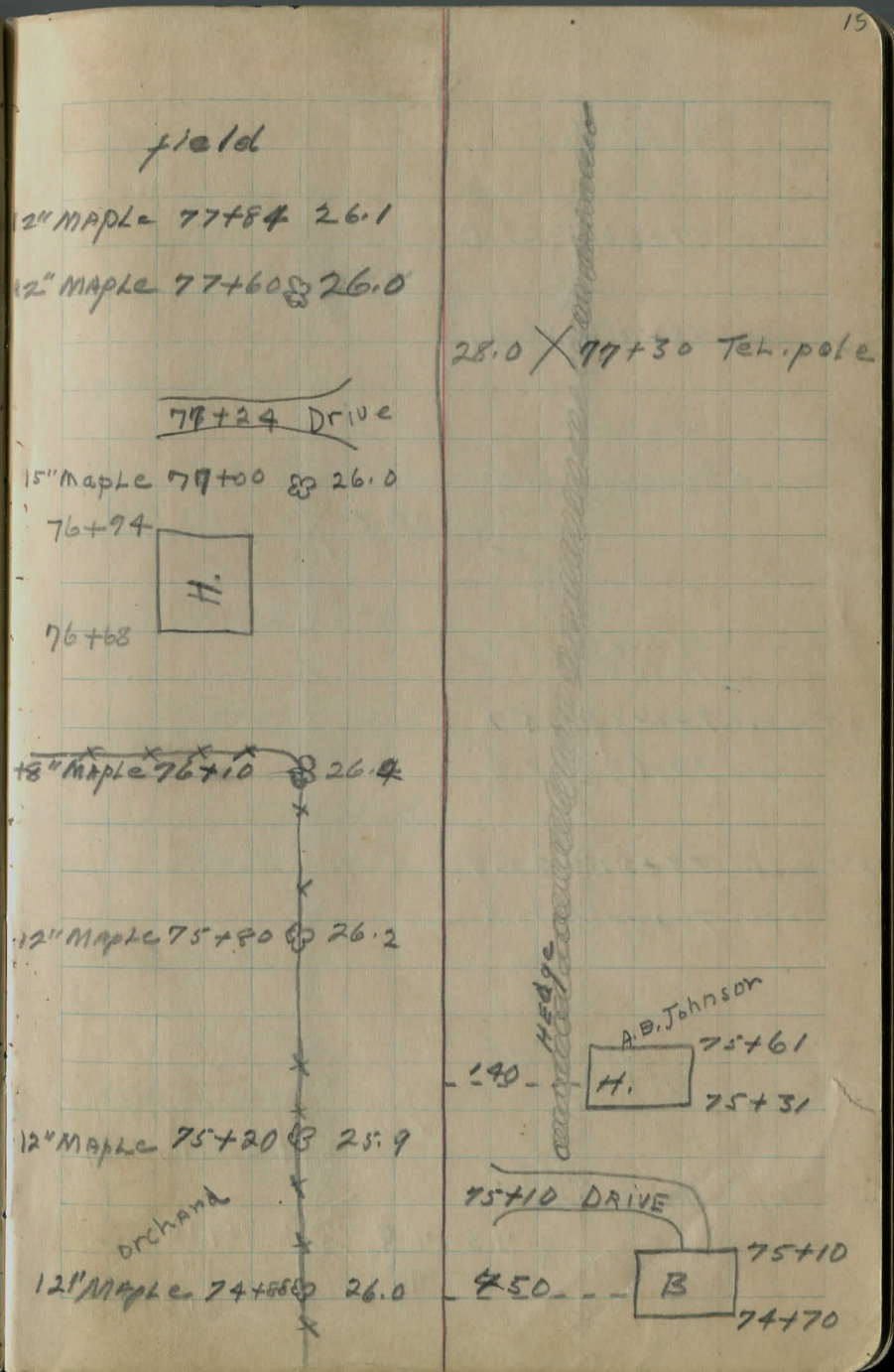

18.0 51+05 20" Maple
Stopped, Aug. 31, 1925
21.5' 49+70
21.2 49+61 24" W. Cherry
25.0 48+91 20" Maple
28.2 48+17 20" Maple
20.4 47+91 12" Elm
27.5 46+68 20" Beech
26' 46+33 16" Elm
Brush & Saplings
24.3 45+98 3-16" Sycamore
13.7 45+61 16" Apple
17.5' 45+36 8" W. Cherry
14.3 44+98 7" Poplar
14' 44+93 12" Elm
13.7 44+80 16" Poplar
48+00
20" Beech 45+93 35.5
12" Beech 45+90 24.5
16" Apple 45+36 18.0
20" Ash
20" Elm
21'
24'
44+48
20" Maple 44+45 21.0
20" Ash, 44+42 15.7

Sept. 1, 1925
Fair-Warm
Reynolds & Parks.






12" Maple 74+59 26.1
orchard.
10" Maple 74+30 24.9
8" Maple 74+00 26.0
13" Maple 73+78 25.9
10" Maple 73+49 25.2
12" Maple 73+20 25.8
10" Maple 75+92 25.7
8" Maple 75+60 25.6
10" Maple 75+35 25.9
corn-field
15" Maple 72+04 25.5
corn-field
12" Maple 71+75 27.2
18" Maple 71+46 25.8
18" Maple 71+15 29.0
29.6 74+35 12" Maple
corn-field
26.8 73+67 12" Maple
25.6 73+00 12" Maple
corn-field
25.7 72+32 10" Maple
corn-field
23.6 71+62 10" Maple
25.1 71+27 12" Maple


field
12" Maple 77+84 26.1
12" Maple 77+60 26.0
28.0 77+30 Tel. pole
77+24 Drive
15" Maple 77+00 26.0
76+94
H.
76+68
18" Maple 76+10 26.4
12" Maple 75+80 26.2
hedge
A.B. Johnson
75+61
H.
75+31
140
12" Maple 75+20 25.9
orchard
75+10 DRIVE
75+10
150
B
74+70
12" Maple 74+68 26.0

8" Maple 82+6 ⊗ 25 4

6" Maple 81+80 ⊗ 25.0

8" Maple 81+48 ⊗ 25.0
25.0

10" Maple 80+29 ⊗ 25.4

28.8 X 80+24 Tel pole

10" Maple 79+98 ⊗ 25.9

8" Maple 79+83 ⊗ 25.2

10" Maple 79+67 ⊗ 25.4

8" Maple 79+52 ⊗ 25.9

6" Maple 79+35 ⊗ 25.8

76+60 DRIVE

78+14 7.3 7.5

HEDGE

Meadow

10" V.P. Culvert

12" Maple 85+98 ⊗ 25.1

6" Maple 85+68 ⊗ 25.5

8" Maple 85+7 ⊗ 25.3

10" Maple 84+78 ⊗ 25.7

8" Maple 84+49 ⊗ 25.5

8" Maple 84+17 ⊗ 25.3

10" Maple 83+87 ⊗ 25.6

10" Maple 83+57 ⊗ 24.8

9" Maple 83+30 ⊗ 25.6

10" Maple 82+98 ⊗ 25.4

Clover field

82+80

Meadow

10" Maple 82+67 ⊗ 25.3

7" Maple 82+35 ⊗ 24.9

HEDGE

29.6 X 85+73 Tel. pole

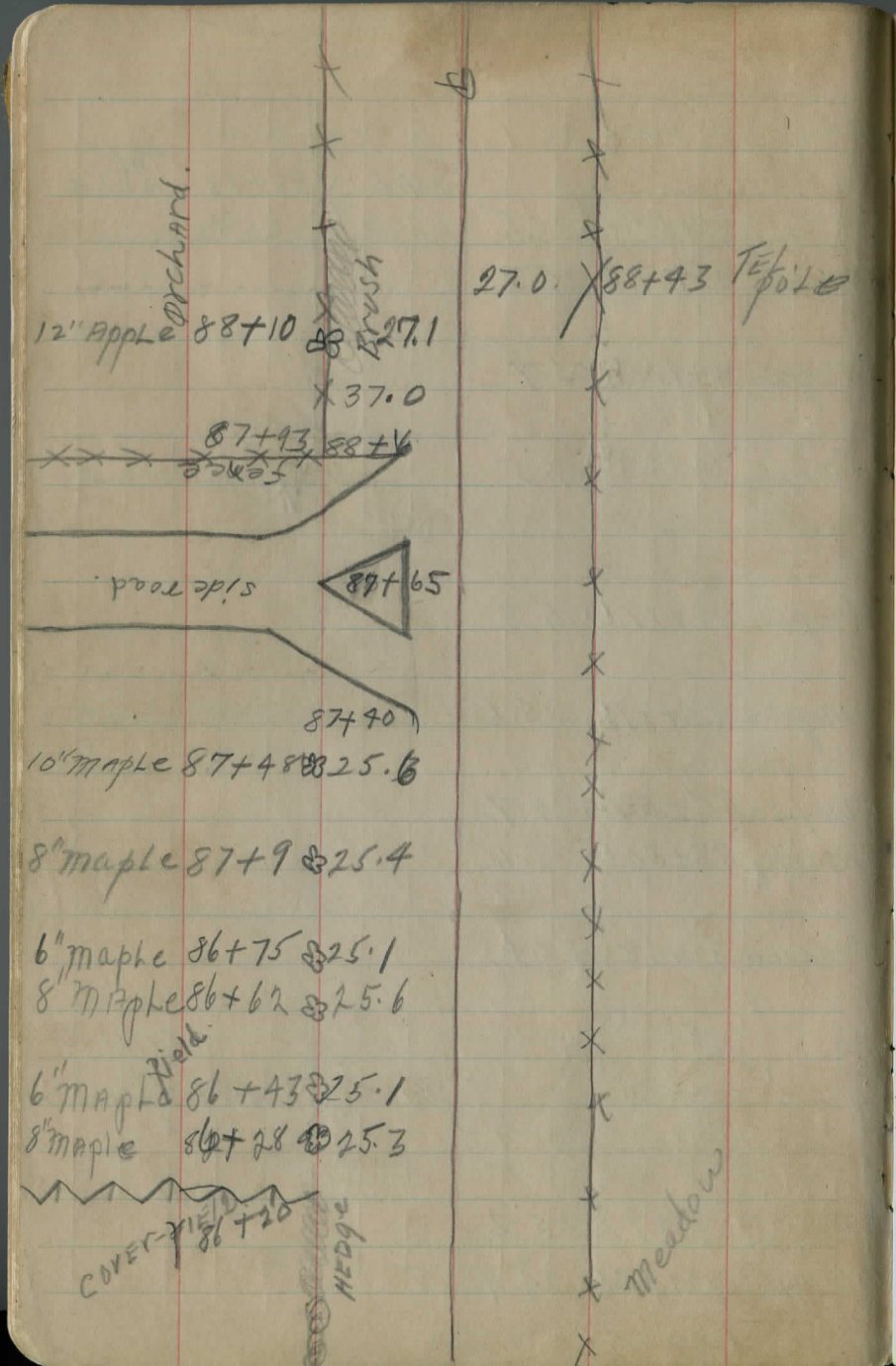
29.9 X 84+70

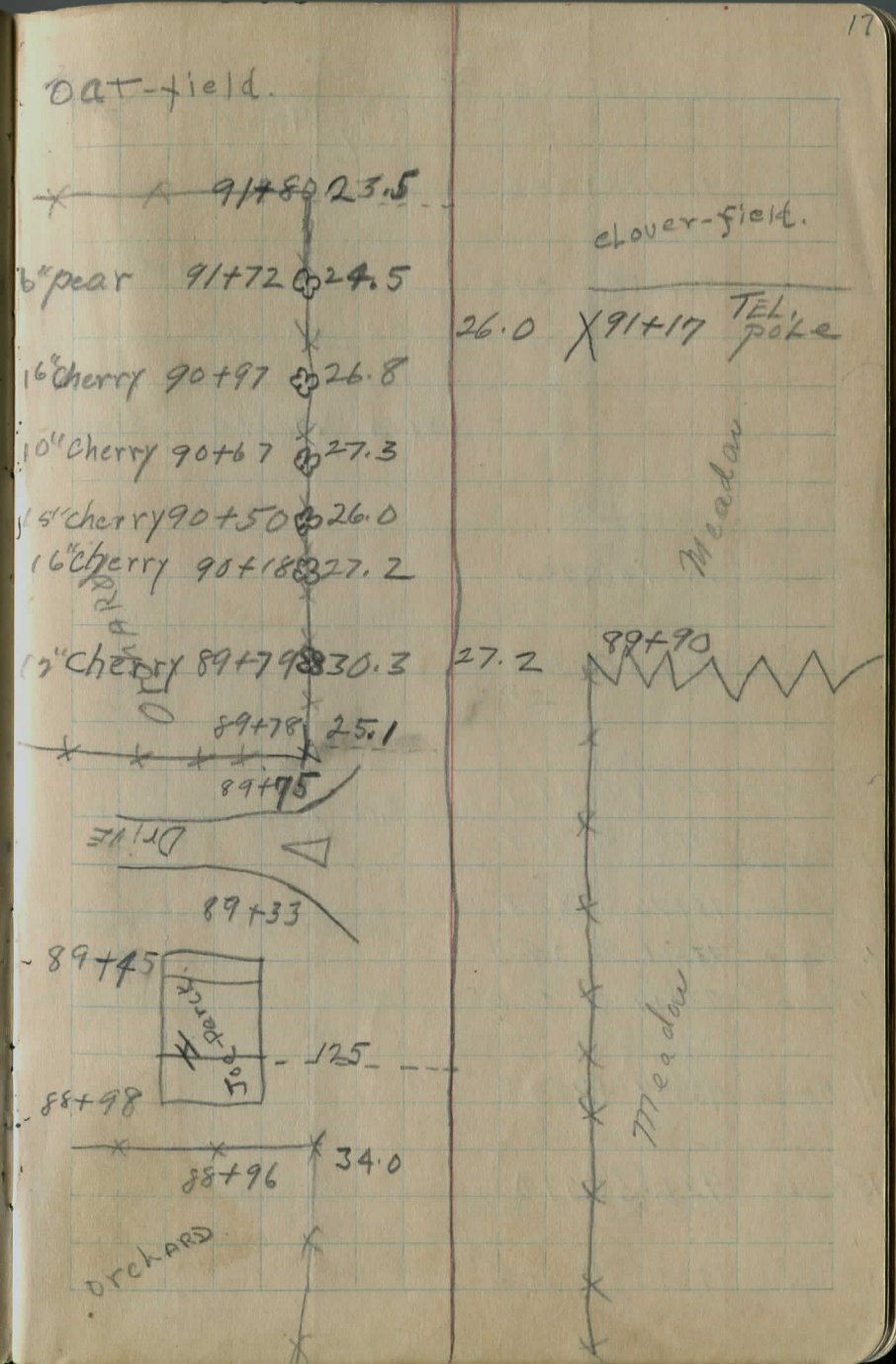
DRIVE 84+40

29.5 X 82+94 Tel pole

HEDGE

Meadow


Orchard
Brush
27.0
88+43
Tel pole
12" Apple 88+10
27.1
37.0
87+93
88+16
side road
89+65
87+40
10" Maple 87+48
25.6
8" Maple 87+9
25.4
6" Maple 86+75
25.1
8" Maple 86+62
25.6
Field
6" Maple 86+43
25.1
8" Maple 86+28
25.3
Cover-field
86+20
Hedge
Meadow


Oat-field.
91+80
23.5
6" pear 91+72
24.5
16" Cherry 90+97
26.8
10" Cherry 90+67
27.3
15" Cherry 90+50
26.0
16" Cherry 90+18
27.2
Road
17" Cherry 89+79
30.3
89+78
25.1
89+75
Drive
89+33
89+45
House
125
88+98
88+96
34.0
Orchard
clover-field.
26.0
91+17
Tel pole
Meadow
27.2
89+90
Meadow

6" Locust 98+98 28.4

15" Apple 98+12 23.6

20" Apple 97+26 24.0

Brush + saplings.

12" Apple 95+13 28.0

18" Apple 94+75 32.6

12" Apple 93+99 29.9

93+92 34.7

18" Apple

8" Apple 93+76 32.3

12" Apple 93+66 24.0

15" Apple 93+47 30.0

16" Apple 92+88 29.8

15" Apple 92+63 29.0

12" Apple 92+25 31.8

28.4 98+85

18' T 98+80

orchard.

28.0 97+00

26.0 X 96+62 Tel. pole

hay-field

25.0 X 93+94 Tel. pole

Meadow.

12" Apple 102+45 37.0

Corn-field.

Bushes.

Hay-field

12" Apple 100+84 31.9

Hay-field.

14" Apple 99+61 25.9

12" Apple 99+52 32.8

13" Apple 99+25 31.3

24.4 X 102+90 Tel. pole

300' B.

24.1 102+39

Drive 102+28

26.0 100+58 8" maple

17.5 T 100+56 garden.

27.4 100+07 8" Elm

100+5

10.0' H

99+76

99+87

300 B.

99+48

27.7 99+46 32" Elm

Drive 99+31

29.4 +99+24

garden

Sept 2, 1925
Fair
Marks
Reynolds
Parks

Stopped Sept. 1, 1925.

106+00 Drive

105+85

H. — 200 —

105+61

22" Apple 105+63 B 25.8

24.9 X 105+58 Tel pole.

26.0 104+52

Ditch 6'

Pond 60' 80'

Garden

104+04 30.3

24.4

117+64 24.9

117+36 24.8

120'
117+00

116+32 25.4

115+00

109+75 500'±

107+38

117+67
30.8

28.8 116+44

30.7 114+88
Large Elms
28.6 114+48

27.2 114+37

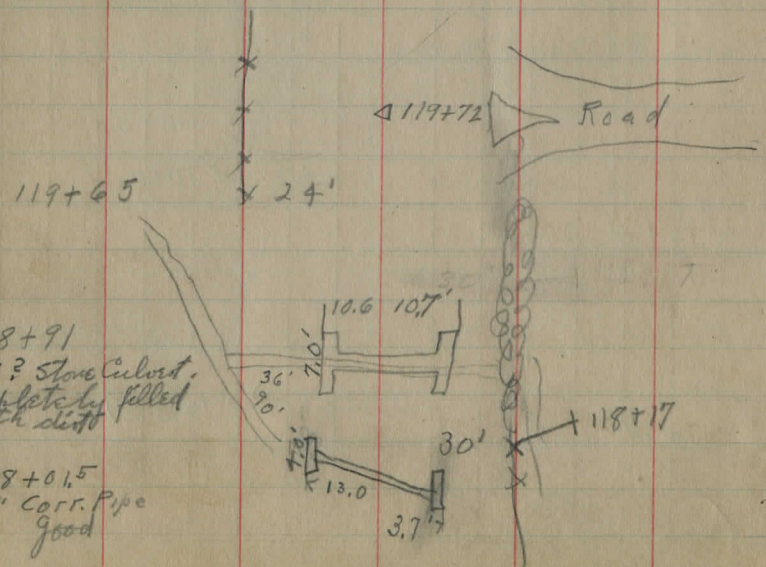
113+20

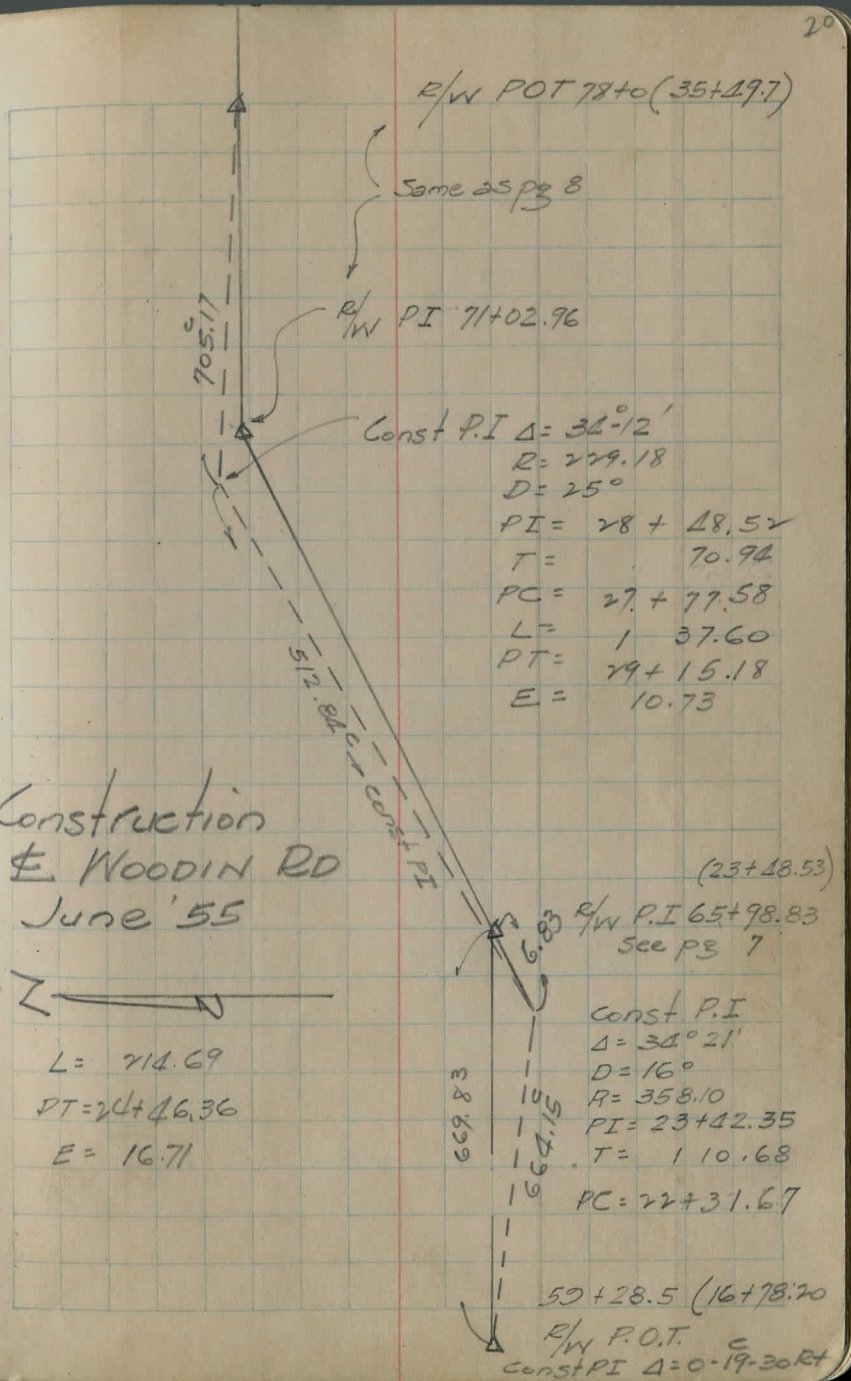
Saplings

111+60
24.2 111+19

23.6 108+86

23.1 108+46


119+72
Road
119+65
24'
10.6
10.7'
7.0'
36'
90°
118+91
3.7 x ? Stone Culvert.
Completely filled
with dirt
30'
118+17
118+01.5
15" Corr. Pipe
Good
13.0
3.7'


R/W POT 78+0 (35+49.7)
Same as pg 8
R/W PI 71+02.96
705.11'
Const P.I Δ = 34°12'
R = 229.18
D = 25°
PI = 78 + 48.52
T = 70.94
PC = 27 + 77.58
L = 1 37.60
PT = 79 + 15.18
E = 10.73
512.84' Const PI
Construction
E. WOODIN RD
June '55
L = 714.69
PT = 24+46.36
E = 16.71
(23+48.53)
R/W P.I 65+98.83
See pg 7
6.83
669.83
664.15
Const P.I
Δ = 34°21'
D = 16°
R = 358.10
PI = 23+42.35
T = 110.68
PC = 22+31.67
59+28.5 (16+78.20
R/W P.O.T.
Const PI Δ = 0-19-30 Rt

				1161.90
				1301.87
	0.80	1162.70		1161.90
	3.79	1161.27	5.22	1157.48
0+00				1156.5
0+25				1156.4
1				1157.8
	8.04	1165.52	3.79	1157.48
1+75				1161.7
2				1161.4
3				1160.6
4				1160.0
5				1159.8
	3.18	1163.04	5.66	1159.86
6				1160.0
7				1159.5

Sept. 2, 1925
Fair. Warm, Dusty

Marks
Reynolds
Parks.

22

2 nails, W. Root, 20" Maple, E. of 62+80, Painesville-Ravenna Road.
W. Root of Walnut, Right 160+05 Old State Road.

2 Nails, W. Root 20" Maple, E. of 62+80 Painesville-Ravenna Rd.
S. W. Cor., S. H.W. Side Road Culvert

6.3/200 6.1/100 4.8/0 2.4/100 0.0/175

6.7/30 6.3/17 5.7/11 5.0/7 4.9/0 4.7/18 6.2/21 5.1/24 4.9/30

1.0/25 1.2/18 3.8/13 4.1/12 3.5/0 4.0/8 4.2/11 3.6/13 2.8/17 1.8/19 2.0/25

3.8/25 3.7/23 2.9/18 4.0/16 5.2/14 4.8/12 3.6/2 3.8/0 4.5/5 5.2/9 3.2/11 1.8/15 1.8/25

4.7/25 4.6/13 4.1/18 4.4/15 5.2/14 5.0/13 3.9/2 4.1/0 4.6/7 5.1/9 4.6/10 3.7/11 2.7/14 2.5/25

5.3/25 5.1/23 4.6/18 4.7/15 5.3/14 5.5/13 4.6/2 4.9/0 5.2/5 5.5/8 5.4/9 4.5/10 3.5/13 2.5/25

5.2/25 5.2/18 5.4/14 6.1/13 6.4/12 6.0/11 5.5/2 5.5/0 5.8/8 6.1/11 5.3/12 4.7/25

6.6/25 6.0/18 6.2/16 6.8/14 6.1/11 5.5/3 5.7/0 6.1/9 6.6/10 5.9/4 5.0/25

3.1/25 3.1/16 3.4/13 3.5/11 2.7/3 3.0/0 3.2/7 2.5/9 0.8/25

4.6/25 3.5/14 4.4/11 3.9/10 3.3/2 3.5/0 3.7/6 4.1/8 3.3/9 2.6/25

		1163.04 ✓		
8				1159.4
9				1158.2
10				1156.4
.	1.92	1158.32 ✓	6.64	1156.40 ✓
11				1153.1
11+50				1150.7
12				1148.3
13				1146.0
	2.59	1148.37 ✓	12.54	1145.78 ✓
14				1143.7
15.				1141.8
16.				1140.8
17.				1140.3
17+08	Sec. for Culvert Design only.			1140.3

6.6 / 25

4.0 / 25 — 4.0 / 16 fence — 4.2 / 17 — 4.5 / 12 — 4.0 / 11 — 3.5 / 3 — 3.6 / 0

4.2 / 8 — 3.6 / 9 — 3.1 / 12 — 3.0 / 25

4.9 / 25 — 5.0 / 14 — 5.4 / 12 — 4.5 / 2 — 4.8 / 6

5.3 / 6 — 5.8 / 7 — 5.0 / 8 — 4.1 / 11 — 3.7 / 25

6.2 / 25 — 6.1 / 16 — 7.2 / 12 — 6.5 / 3 — 6.6 / 0

7.1 / 5 — 7.4 / 6 — 6.2 / 8 — 5.2 / 13 — 5.1 / 25

T.P. 1.P. at 10+00

1.7 / 25 — 1.9 / 20 — 5.9 / 13 — 4.9 / 12 — 5.3 / 10 — 4.8 / 3 — 5.2 / 0

5.6 / 3 — 6.2 / 4 — 5.9 / 6 — 3.8 / 9 — 3.2 / 15 — 3.3 / 25

2.6 / 25 — 3.1 / 21 — 5.4 / 17 — 8.6 / 13 — 7.9 / 11 — 7.2 / 4 — 7.6 / 0

7.9 / 3 — 7.0 / 5 — 6.1 / 9 — 5.6 / 16 — 5.8 / 25

6.3 / 24 — 6.8 / 22 — 10.3 / 13 — 9.7 / 11 — 10.2 / 11 — 9.7 / 3 — 10.0 / 0

10.6 / 6 — 9.6 / 7 — 7.2 / 14 — 9.5 / 25

13.1 / 25 — 12.4 / 17 — 13.2 / 16 — 12.4 / 14 — 12.5 / 13 — 12.3 / 0

12.3 / 3 — 13.3 / 7 — 12.3 / 8 — 12.6 / 11 — 12.0 / 25

4.0 / 25 — 4.3 / 20 — 4.8 / 16 — 4.3 / 14 — 4.9 / 13 — 4.1 / 5 — 4.7 / 0

5.2 / 5 — 5.2 6 — 4.4 8 — 5.4 13 — 1.9 / 25

6.6 / 23 — 6.5 / 17 — 6.9 / 15 — 6.5 / 14 — 6.2 / 4 — 6.6 / 0

~~5.8~~ 7.3 / 8 — 6.4 5.6 / 9 12 — 4.4 / 25

8.4 / 23 — 8.0 / 15 — 8.3 / 14 — 7.6 / 12 — 7.4 / 2 — 7.6 / 0

8.2 / 7 — 8.5 / 9 — 7.4 / 10 — 7.6 / 15 — 7.3 / 25

10.1 / 25 — 9.6 / 15 — 9.8 / 15 — 8.6 / 13 — 8.1 / 0

8.4 / 7 — 9.0 / 10 — 9.6 / 11 — 8.6 / 12 — 7.6 / 23

1132.9 — 1,5,5 / 100

1137.3 — 11.1 / 14.4 F.L.

1140.0 — 8.4 / 12

1140.3 — 8.1 / 0

1140.1 — 8.3 / 7

1138.3 — 10.1 / 8.8 F.L.

1138.8 — 9.6 / 11

1138.8 — 8.6 / 12

1140.3 — 8.1 / 18

1140.7 — 7.7 / 25

		1148.37		
18				1139.5
19				1139.9
	3.21	1142.97	8.61	1139.76
20				1138.2
21				1134.9
22				1131.2
	0.91	1132.12	11.76	1131.21
23				1123.2
	2.57	1121.84	12.85	1119.27
24				1117.9
24+30				1116.6
25				1112.1
	1.36	1110.24	12.96	1108.88
25+50				1106.6
	~~2.72~~	~~1100.57~~	~~12.39~~	~~1097.85~~
26				1103.9
	2.72	1100.57	12.39	1097.85
27				1097.9
28				1095.2

9.6/25 9.1/15 9.7/14 9.1/13 8.9/0

9.1/8 7.7/9 8.9/11 7.6/25

8.4/25 8.5/14 8.9/12 8.5/11 8.2/3 8.5/0

8.9/6 8.0/7 6.7/13 6.1/25

4.4/25 5.1/12 4.5/3 4.8/0

5.1/5 5.5/6 4.6/7 3.6/12 2.8/25

5.7/25 6.3/14 7.0/12 8.8/9 7.9/2 8.1/0

9.1/7 7.2/8 5.0/18 4.8/25

8.5/25 9.2/15 13.3/9 12.4/8 11.8/0

~~11.5~~ 12.3/7 13.5/9 9.6/15 8.5/25

5.0/25 5.3/14 9.0/8 9.0/6 8.9/0

8.9/8 9.2/10 5.9/17 6.0/25

2.0/25 2.9/10 4.0/8 4.5/7 3.9/6 3.9/0 3.8/2 4.2/9 4.5/11 3.2/13 3.4/25

3.2/25 4.1/11 5.9/8 5.3/7 5.2/0

5.4/9 6.0/10 4.8/13 5.3/25

6.2/25 7.3/16 10.8/10 9.5/8 9.7/0

10.0/6 10.5/7 8.9/9 7.5/13 10.1/25

+1.5/25 0.0/17 3.9/10 3.4/9 3.6/0

3.5/5 3.8/6 3.6/8 2.1/11 3.3/25

2.8/25 3.8/15 6.8/10 6.3/9 6.3/0

6.4/8 7.0/9 3.2/14 3.6/25

3.5/25 3.0/8 3.4/7 2.7/5 2.7/0

2.9/7 3.2/12 2.8/11 2.8/25

6.6/25 6.0/7 6.5/6 5.5/4 5.45/0 3.5.5/2 8 5.2/10 5.7/11 5.5/12 4.6/25

		1100.57 ✓		
29				1093.5
29+10		For Culvert Design Only		1093.4
30				1093.2
			3.16	1097.41 ✓
~~37~~				
31				1093.8 ✓
	13.10	1106.91 ✓	6.76	1093.81
32				1094.2
32+50				1095.0
33				1096.2
33+50				1097.4
34				1099.2
34+50				1100.9
35				1096.0
			11.84	1095.07 ✓

7.5/25 8.3/7 7.2/6 7.1/0 — 7.0/2 — 7.6/11 8.9/13 9.5/25

1092.7 1092.6 1091.8 1091.8 1092.7 1093.3 1093.4 1093.6 1093.1 1091.5 1091.2 1089.0

7.9/25 8.2/9 8.8/8 8.8/6.7 F.L. 7.9/6 7.3/4 7.2/0 7.0/2 7.5/11 9.1/11.7 F.L. 9.4/25 11.6/100

6.8/25 7.4/8 7.9/6 7.4/5 7.4/0 — 7.2/4 — 7.4/13 7.7/14 6.9/15 7.4/25

B.M.
R.P. Spike, 10" Tulip Tree, Left of 30+84

7.2/25 7.2/8 7.2/5 6.8/0 — 7.0/12 7.3/13 7.1/14 7.3/16 7.5/25

12.8/25 12.9/9 13.3/8 13.0/7 12.7/0 12.6/2 — 13.0/10 13.5/12 13.2/13 13.8/25

12.4/25 12.4/8 12.2/7 11.9/0 — 12.1/9 12.6/10 12.3/11 13.5/25

10.7/25 10.7/10 11.1/9 10.7/0 — 11.1/6 11.3/7 8.2/12 5.0/25

8.7/25 9.3/9 9.8/7 9.5/0 — 9.7/7 10.2/9 8.9/10 8.6/25

3.2/25 4.1/12 7.8/8 7.7/0 — 7.5/2 8.0/8 7.0/10 6.3/12 7.0/25

0.6/25 1.1/21 3.9/12 6.0/9 6.4/8 6.0/5 6.0/0 — 6.4/9 6.9/10 4.4/13 4.1/25

4.2/25 4.7/19 8.3/12 10.8/7 10.8/6 10.9/0 — 10.9/7 9.8/9 9.6/11 12.6/25

Top of
T. P. Offset Stake, 25' R. 35+00

	2.16	1097.23		1095.07
36+00				1085.0
36+50				1082.2
37				1079.6
	0.69	1085.00	12.92	1084.31
36+50				1082.2
37				1079.6
38				1073.5
	0.97	1074.51	11.46	1073.54
39				1070.6
40				1067.9
41				1065.4
42				1064.0
42+12	Bridge Floor		10.5	1064.0
42+31	Stream Bed		22.5	1052.0
42+50	Bridge Floor		10.8	1063.7

Sept. 3, 1925
Cool, Cloudy, Muddy

Marks, Reynolds
Parks

Top of Stake, 25' R. of 35+00

5.8 / 25	7.1 / 19	12.5 / 9	12.1 / 8	12.2 / 0	12.6 / 4	12.3 / 6	11.9 / 7-9	16.0 / 18	16.2 / 25
9.4 / 33	10.5 / 28	12.6 / 22	14.5 / 13	15.0 / 0					
12.3 / 30	13.5 / 18	15.1 / 11		17.6 / 0					
2.2 / 13	2.8 / 12	3.0 / 10	2.7 / 8	2.8 / 0	2.9 / 6	2.8 / 8	4.7 / 14	5.0 / 25	
0.4 / 25	2.8 / 11	5.5 / 7	5.2 / 5	5.4 / 0	5.6 / 7	5.8 / 9	4.9 / 10	5.7 / 25	
9.4 / 25	12.2 / 11	11.5 / 5	11.5 / 0				11.5 / 6	12.0 / 11	12.4 / 25
4.5 / 25	4.4 / 11	4.7 / 10	4.4 / 9	3.9 / 6	3.9 / 0		4.0 / 7	4.0 / 9	5.4 / 16	6.1 / 25
6.2 / 25	6.4 / 12	7.2 / 10	6.7 / 7	6.6 / 0		6.7 / 6	7.1 / 8	5.3 / 9	5.0 / 16	5.7 / 25
9.7 / 25	10.0 / 9	9.6 / 6	9.1 / 0				9.4 / 8	8.6 / 17	12.5 / 25
19.5 / 25	13.3 / 15	10.3 / 11	10.2 / 5	10.5 / 2	10.5 / 0		10.6 / 6	10.8 / 12	11.5 / 25

		1074.51		
	5.52	1068.70	11.33	1063.18
			7.02	1061.68
43				1062.2
43+15	Profile, Road North			1062.6
44			3.2	1065.5
+35			1.9	1066.8
+50			1.1	1067.6
	10.95	1079.33	0.32	1068.38
45			8.3	1076.0
+56			3.2	1076.1
	12.84	1092.17	0.00	1079.33
46			8.7	1083.5
+50			1.2	1091.8
	11.57	1103.74	0.00	1092.17
47			6.4	1097.3
+50			2.0	1101.7
	8.73	1112.47	0.00	1103.74
48				1104.9
~~47~~			0.80	1111.67

B.M. Set, Spike, E. Root 16" Walnut 825' L. of Sta. 42+90

7.7 / 25 | 6.5 / 0 | 6.3 / 8 | 7.3 / 10 | 9.5 / 15 | 9.8 / 25

6.7 / 200 | 7.4 / 100 | 7.0 / 50 | 6.9 / 18 | 6.1 / 7 | 6.1 / 0

2.9 / 25 | 5.0 / 14 | 7.7 / 8 | 8.4 / 7 | 8.1 / 6 | 7.6 / 0 | 7.6 / 8 | 7.9 / 9 | 6.2 / 12 | 4.4 / 25

B.M. set, R.P. spike, 20" Maple, R. 48+91

44

44+35 For Culvert Design

44+50

45

45

45+50

46

46

46+50

46+50

47

47

47+50

$\frac{5.5}{25}$ $\frac{5.4}{9}$ $\frac{5.9}{8}$ $\frac{5.3}{5}$ $\frac{5.3}{0}$ $\frac{5.5}{11}$ $\frac{8.7}{18}$ $\frac{9.4}{25}$

$\frac{9.0}{25}$ $\frac{9.5\ 8.1\ 4.5}{11.3}$ $\frac{4.9}{0}$ $\frac{4.9-8.1-9.5}{5.4}$ $\frac{9.5}{25}$

$\frac{6.5}{25}$ $\frac{5.9}{18}$ $\frac{5.5}{10}$ $\frac{5.3}{0}$ $\frac{5.6}{4}$ $\frac{6.9}{11}$ $\frac{7.6}{17}$ $\frac{6.8}{20}$ $\frac{6.5}{25}$

$\frac{10.0}{0}$ $\frac{10.3}{5}$ $\frac{11.0}{7}$ $\frac{10.0}{8}$ $\frac{3.3}{18}$ $\frac{1.4}{22}$ $\frac{1.3}{25}$

$\frac{5.0}{25}$ $\frac{4.4}{19}$ $\frac{6.0}{16}$ $\frac{6.0}{14}$ $\frac{6.4}{13}$ $\frac{5.5}{10}$ $\frac{5.6}{0}$

$\frac{2.8}{25}$ $\frac{2.4}{11}$ $\frac{4.0}{8}$ $\frac{5.0}{0}$ $\frac{5.1}{8}$ $\frac{5.7}{11}$ $\frac{4.3}{12}$ $\frac{3.1}{13}$ $\frac{1.5}{18}$ $\frac{1.6}{25}$

$\frac{7.0}{0}$ $\frac{5.8}{8}$ $\frac{3.8}{12}$ $\frac{5.5}{16}$ $\frac{4.2}{19}$ $\frac{5.5}{25}$

$\frac{+0.7}{35}$ $\frac{0.0}{28}$ $\frac{10.6}{10}$ $\frac{13.7}{8}$ $\frac{13.2}{6}$ $\frac{13.0}{0}$

$\frac{11.4\ 11.6\ 2.0}{0\ 5\ 6}$ $\frac{5.5}{12}$ $\frac{3.1}{17}$ $\frac{3.3}{22}$ $\frac{4.1}{25}$

$\frac{+0.8}{30}$ $\frac{+0.8}{26}$ $\frac{14.1}{9}$ $\frac{13.6}{6}$ $\frac{13.2}{0}$

$\frac{10.1}{0}$ $\frac{10.0}{7}$ $\frac{10.3}{8}$ $\frac{5.5}{12.5}$ $\frac{3.2}{16.5}$ $\frac{4.4}{25}$

$\frac{0.4}{35}$ $\frac{0.1}{30}$ $\frac{0.3}{28}$ $\frac{2.3}{23}$ $\frac{5.5}{16.5}$ $\frac{12.2}{8.5}$ $\frac{11.5}{6}$ $\frac{11.0}{0}$

Averages between 47+00 + 48+00

	4.73	1116.42		1111.67
49				1109.5
50				1112.9
	8.08	1124.25	0.25	1116.17
51				1116.8
52				1119.5
53				1123.2
	11.15	1135.40	0.00	1124.25
53+50				1125.3
54				1129.5
	10.26	1144.00	1.66	1133.74
54+50				1133.0
55				1137.3
	11.58	1154.64	0.94	1143.06
56				1142.9
57				1147.8
	12.97	1165.96	1.65	1152.99

B.M. Right 48+91

3.5	4.1	7.0	7.9	7.2	6.9	7.2	7.8	6.8	5.7	6.4
25	18	12	11	8	0	6	8	10	14	25
4.0	3.3	4.1	3.7	3.5		3.7	4.2	7.8	2.2	
25	10	9	8	0		5	7	9	25	
8.8	8.8	9.2	8.2	8.0		8.4	8.9	7.7	7.2	7.7
25	11	10	6	0		5	8	10	17	25
5.1	5.4	6.0	5.2	4.8		5.3	5.6	5.1	5.7	
25	11.5	10	8	0		6	8	9	25	
+1.3	0.6	2.1	1.6	1.1		1.8	2.3	1.5	0.6	0.7	0.9
25	12	8	6	0		8	9	10	15	20	25
5.2	6.3	10.9	10.2	10.1		10.1	10.4	11.1	7.1	7.8	
25	14	8	5	0		4	7	10	15	25	
2.0		4.2	5.9			6.3	7.0	3.0	3.6		
25		17	0			8	10	16	25		
6.9	8.0	11.5	11.1	11.0		11.3	12.3	8.6	8.2		
25	12	7	6	0		7	11	16	25		
3.0	4.0	7.8	6.9	6.7		7.0	7.2	8.4	5.1	4.2	
25	13	6	5	0		4	6	9	14	25	
10.0	10.7	12.5	11.8	11.7		11.8	12.3	10.7	10.2		
25	9	7	4	0		4	9	12	25		
4.7	5.9	7.7	7.2	6.8		7.1	7.9	5.6	4.9		
25	10	8	6	0		6	9	13	25		

		1165.96		
58			1153.3	
59			1160.2	
			0.14	1165.82
	0.69	1166.51		1165.82
60			1164.1	
	10.35	1176.86	0.00	1166.51
60+42	Section for Culvert Design only			1165.7
61			1167.6	
62			1170.7	
63			1173.8	
	11.41	1188.27	0.00	1176.86
64			1177.4	
65			1183.7	
	11.99	1200.26	0.00	1188.27

10.1/25 11.4/11 13.3/9 12.9/7 12.7/0 12.6/5 13.0/7 8.8/14 7.8/25

5.1/25 4.0/12 6.2/8 5.9/7 5.8/0 5.7/5 6.0/7 4.2/11 3.7/25

B.M. set. R.P. spike, Right, 59+28.5
Stopped, Sept. 3, 1925

Sept. 4, 1925 Marks, Reynolds, Parks.
Fair.

B.M. R. 59+28.5

3.8/25 3.4/22 3.1/11 3.6/10 2.7/7 2.4/0 2.8/3 3.7/8 2.9/9 1.7/13 0.6/25

1161.3 15.6/60 1163.9 13.0/9.8 11.5/8 1165.4 11.2/0 1165.7 11.1/5 1165.8 12.3/6.9 F.L. 1166.0 10.9/10 1166.8 10.1/13 1167.6 9.3/25

10.0/25 9.7/12 10.2/11 9.5/4 9.3/0 9.4/4 9.8/6 10.7/8 8.7/10 7.2/14 7.6/30 7.3/25

8.2/25 6.7/11 7.7/10 6.8/6 6.2/0 6.5/5 7.2/9 5.5/12 4.8/25

6.9/25 5.4/19 4.0/9 4.4/8 3.7/5 3.1/0 3.3/6 3.9/9 1.5/14 0.2/25

9.6/25 10.2/11 11.5/8 11.1/6 10.9/0 11.2/6 12.0/9 8.7/14 8.0/25

1.9/25 2.0/14 5.2/9 5.0/6 4.6/0 5.0/5 6.1/9 3.2/11 2.4/13 2.8/15 2.9/25

		1200.26		
65+50				1186.4
66				1189.2
66+50				1191.6
67				1194.1
	11.18	1211.44	0.00	1200.26
68				1200.0
	11.18	1211.44	0.00	1200.26
69				1209.4
	12.12	1222.94	0.62	1210.82
	12.32	1235.22	0.04	1222.90
70				1223.7
70+10			9.7	1225.5
70+45			5.4	1229.8
70+60			3.5	1231.7
			1.01	1234.21
	10.92	1245.03	1.11	1234.11
71				1234.1
71+50				1237.6

12.0/25 12.4/13 9.3/8 14.1/7 13.9/0 — 14.2/7 15.6/11 12.4/13 11.9/14 12.2/16 12.5/25

10.5/24 10.1/20 9.8/13 10.6/10 11.1/0 — 10.8/9 12.0/19 11.3/21 9.8/25

1190.1 1191.5 1190.5 1191.0 1191.6 — 1191.4 1190.3 1192.8 1193.2

10.2/25 8.8/16 9.8/12 9.3/8 8.7/0 — 8.9/8 10.0/13 7.5/14 7.1/25

7.5/25 6.2/14 7.7/13 7.3/9 6.2/0 — 6.6/9 7.4/11 7.1/14 5.4/16 5.1/25

11.0/25 10.7/14 11.6/12 11.9/11 11.6/9 11.4/8 11.4/0 — 11.4/10 12.5/11 12.3/15 8.7/18 8.2/25

1.0/25 0.7/14 2.3/11 2.0/9 2.0/0 1.8/10 2.9/11 1.5/14 — +0.6/19 +1.5/25

12.0/25 12.0/19 12.4/16 13.1/14 11.9/12 11.5/0 — 10.8/9 11.4/11 9.3/14 8.4/17 7.8/25

2.3/30-25 2.4/21 4.0/17 4.6/15 4.0/13 3.0/8 3.5/0 — 4.1/7 4.8/9 3.7/11 0.8/18 0.6/21 0.0/23 c. of tree

B.M. Set. S. root 20" Maple, Left 70+75

T.P. R.I. Hub.

7.6/32 — 8.0/22 11.3/13 10.9/9 10.9/0 — 11.4/5 11.5/8 8.1/12 7.0/15 6.4/25

3.9/26 4.9/17 5.7/13 8.2/9 7.6/8 7.4/0 — 7.5/8 8.1/9 5.2/12 4.7/25

		1245.03		
72				1241.8
	12.85	1257.88	0.00	1245.03
73				1247.8
74				1252.3
75				1256.5
	11.36	1268.02	1.22	1256.66
76				1260.8
	10.95	1276.47	2.50	1265.52
77				1265.7
78				1269.3
				1269.8
78+14	Section for Culvert design only			
			4.28	1272.19
79				1272.0
80				1272.5
81				1273.0
82				1273.2

1.0/25 2.1/13 3.5/9 4.0/8 4.3/7 3.7/5 3.2/6

3.4/8 3.7/9 3.6/11 2.2/12 1.6/25

7.9/25 9.1/12 11.8/7 10.7/6 10.1/0

10.5/7 11.0/10 10.1/11 10.0/25

3.4/25 4.9/14 6.0/12 6.3/11 6.1/9 5.6/0

5.9/6 6.5/7 5.8/9 7.1/25

+2.0/25 +0.6/19 0.4/14 1.6/12 1.5/10 1.2/3 1.4/0

2.1/4 2.4/6 1.7/7 1.6/25

4.3/25 5.5/14 7.2/12 7.0/10 7.1/3 7.2/0

7.5/7 8.1/6 5.8/8 5.3/25

8.5/25 8.8/12 10.6/10 10.7/8 10.8/0

11.2/5 11.3/8 10.1/10 8.8/25

6.9/25 7.2/10 7.6/9 7.3/7 7.2/0

7.6/6 8.2/8 7.8/9 8.3/25

1269.5 1269.0 1268.5 1269.5 1269.8 1269.3 1268.5 1268.1 1264.8

7.0/25 7.5/10 8.0/7.3 7.0/6 6.7/0 7.2/7 8.0/7.5 8.4/25 11.7/100

Top of stake, 25' R. 79+00

3.6/25 4.7/8 6.3/7 5.9/5 5.5/0

5.2/2 5.9/8 6.6/10 5.7/12 5.3/25

3.0/25 3.9/9 5.2/8 4.3/6 4.0/0

3.8/2 4.5/9 5.2/10 4.5/11 4.8/25

3.4/25 3.6/21 4.0/11 4.8/10 3.5/7 3.5/0

3.4/2 4.0/10 4.5/11 4.9/12 4.4/25

2.0/25 2.9/21 3.8/10 4.3/9 3.6/7 3.3/0

3.2/3 3.7/10 4.5/12 3.8/13 4.4/25

		1276.47		
83				1274.0
	3.37	1277.94	1.90	1274.57
84				1274.5
85				1275.1
86				1275.1
87				1275.3
87+65	℄ Road North			1274.4
88				1273.5
			3.55	1274.39
89				1271.0
90				1266.7
	1.56	1267.40	12.10	1265.84
91				1262.3
92				1259.0
93				1254.6

2.2/23 3.1/12 3.7/11 2.9/9 2.5/0 — 3.0/9 3.7/10 2.9/12 3.0/25

3.6/22 4.1/12 4.7/11 3.9/9 3.4/0 — 3.8/7 4.6/9 4.1/11 4.3/25

2.8/23 3.2/13 3.8/12 3.2/10 2.8/0 — 3.3/6 4.1/8 3.6/9 3.3/25

2.6/23 3.3/13 3.9/12 3.1/10 2.8/0 — 3.2/6 3.9/8 3.5/9 3.4/25

2.2/25 2.6/9 3.4/8 2.9/7 2.6/0 — 2.9/7 3.4/9 3.1/10 3.0/25

2.5/150 2.9/100 3.2/50 3.2/10 4.1/9 3.8/7 3.5/0 — 3.8/7 4.2/9 3.6/10 3.5/25

3.1/25 4.0/9 5.1/8 4.7/7 4.4/0 — 4.7/7 5.1/9 4.4/11 4.4/25

B.M. Set Spike, S.E. Root 18" Maple, L. 88+85

5.1/25 6.3/11 7.5/9 6.9/0 — 7.3/6 7.9/8 6.7/10 7.0/25

9.3/25 11.5/10 12.3/9 12.4/8 11.6/7 11.2/0 11.0/1 — 11.7/9 12.4/10 11.2/12 11.3/25

3.2/14 fence 3.9/18 4.7/17 5.5/10 6.1/9 5.4/7 5.1/0 — 5.5/8 6.3/10 5.6/12 6.2/25

7.0/25 7.5/21 9.1/12 10.2/10 9.1/8 8.4/0 — 9.2/8 10.3/11 8.8/13 8.8/25

10.7/25-20 12.7/16 13.7/11 14.8/10 13.5/9 12.8/0 — 13.3/8 14.8/10-11 12.9/12 12.2/25

		1267.40		
	0.83	1256.39	11.84	1255.56
94				1248.7
~~95~~				
	1.29	1244.84 ~~1245.84~~	12.84	1243.55 ~~1244.55~~
95				1242.2
96				1234.8
	1.99	1234.30 ~~1235.30~~	12.53	1232.31 ~~1233.31~~
97				1228.0
98				1222.5
	0.51	1222.38 ~~1223.38~~	12.43	1221.87 ~~1222.87~~
99				1216.8
			5.57	1216.81 ~~1217.81~~
100				1211.2
	1.76	1211.18 ~~1212.18~~	12.96	1209.42 ~~1210.42~~
101				1207.3
102				1204.2
103				1201.4 ~~1201.4~~

5.7/25-20 7.4/17 7.4/13 9.4/11 8.4/9 7.7/0

8.3/8 9.2/11 6.3/15 5.6/25

~~11.7/23 11.9/21~~

~~11.9/15 12.1/23~~

0.1/25 0.3/22 2.7/20 2.3/14 4.3/12 4.8/11 3.1/9 2.6

3.1/8 4.3/11 5.6/13 0.3/15 0.4/25

7.8/25 7.9/22 10.1/14 12.1/13 10.4/9 10.0/0

10.2/8 11.0/12 8.9/14 8.8/25

3.8/25 4.1/20 5.6/18 6.1/15 8.1/12 6.6/11 6.3/0

6.5/10 8.4/13 5.4/14 5.3/25

8.9/25 9.0/23 11.3/18 12.9/14 13.7/13 12.2/12 11.8/0

12.1/9 13.3/12 11.4/14 11.1/25

3.4/25 4.8/20 5.7/16 7.4/15-14 6.1/12 5.6/0

5.8/9 6.5/12-13 5.5/14 4.6/25

B.M. set, Large Elm, Right 99+45

9.2/25-24 11.1/19 11.5/15 12.7/12 11.8/12 11.2/0

11.2/7 12.8/10-11 10.4/14 9.8/25

2.6/25 4.0/13 5.4/12 4.6/11 3.9/0

4.3/8 4.7/11 3.7/13 2.9/25

6.8/25 6.8/19 7.3/13 8.4/12 7.5/9 7.0/0

7.7/8 8.0/10-11 7.1/13 6.3/25

9.3/25 9.8/15 10.8/13 10.3/12 7.8/0

10.4/7 11.1/9 10.2/10 9.0/25

		1211.18 ~~1212.18~~		1199.0
104				
	3.30	1201.56 ~~1202.56~~	12.92	1198.26 ~~1199.26~~
			4.62	1196.94 ~~1197.94~~
	3.96	1200.90 ~~1201.90~~		1196.94 ~~1197.94~~
~~105~~				
105				1198.0
~~106~~				
106				1195.6
~~107~~				
107				1194.2
~~108~~				
108				1192.7
				1190.7
109		1193.69 ~~1194.69~~		1191.45 ~~1192.45~~
	2.24		9.45	
110				1189.6
111				1188.9
112				1188.4
113				1187.7
114				1187.3

12.1/25 12.4/14 13.2/13 12.7/11 12.2/0 — 12.6/5 13.1/7 12.2/8 12.7/25

B. M. set, S.W. cor. 22" Apple, Left 105+63
Sep. 5, 1925, Fair. Warm. Marks, Raynolds, Parks
B. M. 105+63

3.9/25 4.0/15 4.9/13 4.3/11 3.7/3 3.9/0 — 4.4/4 4.8/5 5.0/7 3.9/8 3.9/13 2.7/15 1.2/25

5.8/25 5.1/14 5.9/13 5.4/12 5.2/3 5.3/0 — 6.0/6 6.6/7 5.3/9 4.5/25

6.9/25 6.9/16 8.0/15 7.1/12 6.4/3 6.7/0 — 7.2/4 7.9/6 6.2/7 6.7/10 6.3/25

7.1/25 7.6/18 9.4/16 8.5/13 7.8/5 8.2/0 — 8.6/4 9.6/6 7.8/7 8.1/9 8.0/25

9.5/25 9.9/17 10.7/16 9.9/13 9.5/6 10.2/0 — 10.5/2 10.8/4 9.9/5 9.1/25

4.0/25 3.7/20 4.3/19 3.6/5 4.1/0 — 4.5/3 3.7/11 4.4/25

5.1/25 4.7/20 5.2/19 4.4/7 4.8/0 — 5.1/2 5.5/4 4.6/5 5.3/16 5.5/25

5.7/25 5.4/19 6.1/18 5.6/16 4.9/6 5.3/0 — 6.6/2 6.2/5 5.5/6 4.1/12 3.1/25

6.7/25 6.3/18 7.0/17 6.3/14 5.7/6 6.0/0 — 6.1/4 7.0/6 6.1/7 6.9/25

7.5/25 7.2/17 7.7/16 6.9/14 6.2/6 6.4/0 — 6.6/5 7.6/7 6.7/8 7.4/25

Sta.	+	H.I.	−	El.
		1193.69 ~~1194.69~~		1187.41 ~~1188.41~~
	3.42	1190.83 ~~1191.83~~	6.28	
115				1186.8
116				1185.3
117				1184.9
118				1185.2
118+01.5				1185.2
118+50				1185.2
118+91	Section for Culvert Design only			1185.9
119				1185.8
119+72	℄ Road to South			1186.2
120			4.2	1186.6
+50			2.9	1187.9
121			2.3	1188.5
+50			0.9	1189.9
+80			0.0	1190.8

B.M. set. Spike, N. root Large Elm R. 114+48

4.0/25 5.0/17 5.6/16 4.9/13 3.7/5 4.0/0

4.8/7 5.5/8 4.7/10 4.7/25

6.1/25 5.7/16 6.0/15 5.8/13 5.5/0

6.1/8 6.6/9 6.0/10 5.0/25

6.7/25 6.3/16 7.0/15 6.3/12 5.9/0

6.6/8 7.3/9 6.4/11 7.1/25

6.4/25 6.9/17 7.7/16 6.1/13 5.4/5 5.6/0

6.0/3 7.3/8 7.4/25

1183.1

8.8/250 7.9/150 7.5/90 8.0/50 7.7 F.L. 6.4-5.5/13.0 5.8/12.0 5.6/0 5.8/2.7

1183.2

5.3-6.3-7.6/3.7 F.L. 7.4/25

6.7/25 7.5/21 6.8/20 6.7/17 6.9/15 6.0/13 5.3/3 5.6/0

5.8/3 7.0/7 7.3/25

1183.9

7.6/36 6.9 6.9-4.1/10.6 5.2/9 4.9 5.1/9

4.2-6.7-6.7/10.7 6.6/17 5.5/19 5.9/21 2.7/28

6.1/25 6.4/15 5.3/9 5.0/0

5.2/7 5.6/11 5.6/21 3.2/25

5.1/25 5.1/17 5.4/16-13 4.8/8

4.6/6 4.4/11 4.0/20 3.3/21 3.5/50 1.3/100 0.0/130

	1190.83 ~~1191.83~~		
9.34	1199.47 ~~1200.47~~	0.70	1190.13 ~~1191.13~~
		0.11	1199.36 ~~1200.36~~
11.44	1210.80 ~~1211.80~~		
+		0.00	1210.80 ~~1211.80~~
12.87	1223.67 ~~1224.67~~		
		0.00	1223.67 ~~1224.67~~
10.19	1233.86 ~~1234.86~~		
		0.00	1233.86 ~~1234.86~~
10.20	1244.06 ~~1245.06~~		
		11.19	1232.87 ~~1233.87~~
12.17	1245.04 ~~1246.04~~		
		1.19	1243.85 ~~1244.85~~
13.10	1256.95 ~~1257.95~~		
		0.83	1256.12 ~~1257.12~~
10.56	1266.68 ~~1267.68~~		
		0.87	1265.81 ~~1266.81~~
12.40	1278.21 ~~1279.21~~		
		0.71	1277.50 ~~1278.50~~
12.26	1289.76 ~~1290.76~~		
		0.77	1288.99 ~~1289.99~~
10.02	1299.01 ~~1300.01~~		
		1.51	1297.50 ~~1298.50~~
5.56	1303.06 ~~1304.06~~		
		1.58	1301.48 ~~1302.48~~

1301.87 Spike, W. Root, Walnut, Right 1160+05 Old State Road.

Fiddler x Dirty April 28th 1926
cloudy - rain 10:20 to 11 [illegible]

143 quit at rain - 2 spikes on ℄ for [only measured]

142

141

140

139

138

137+42.75 Pg plank spike on Tangent

187

136

135

134 no stake set on offset line

133+98.1 P.I. 0° △ 35' ℄ L. Spk F6 MAY 55

+42.75 = 9.41

Cont. from 10

127+60

Aug. 21, 1957
Warm - FAIR - AM
RAIN - PM

CANFIELD
ADAMS

L R

39

maple
nail in W. root.
21.15'
25'
sta. 8 stake

spike SW on S.E. side
12" maple 8" n/s

IP set 8-21-57 Fl 05 H

I Pin set in Pavem't
8-10-55 VERT SCW N ROOT
12" CHERRY

15.0'

26.55

bent spike SW on E side 26" maple 8" n/s.

25.78

I.P.N SET P.O.T MAY '55

39.83

VERT SCW N.E. ROOT
14" MAPLE

IP set Fl 05 H
8-21-57

Gone
spike in S.E. side 12" Maple

SCW E. CEI 567036

38.0'

I Pin set in pavem't 8-10-55

SCW NE 12" ASH

BOULDER
in Head of Spn

29.50

38.54

IP IPF F6:

29.93

23.5'

No FIND MAY 55

1" steel pipe tube 21" long set 4" below surface.

spike in W. root 10" Maple

38.78

SCW NW 10" ELM

Profile Line Lawrence
Kish

KISH

Fiedler + Dietz 4/28-26

+ 193.8 iron pipe on Tang.
155

154

153

152

151

150

149

Concrete Culvert (Ext. both ways, Highways Gone)

+ 41.1 I.P. △ 0°-32' R. No Find I.P. Spk Set 6-3-55

148

+

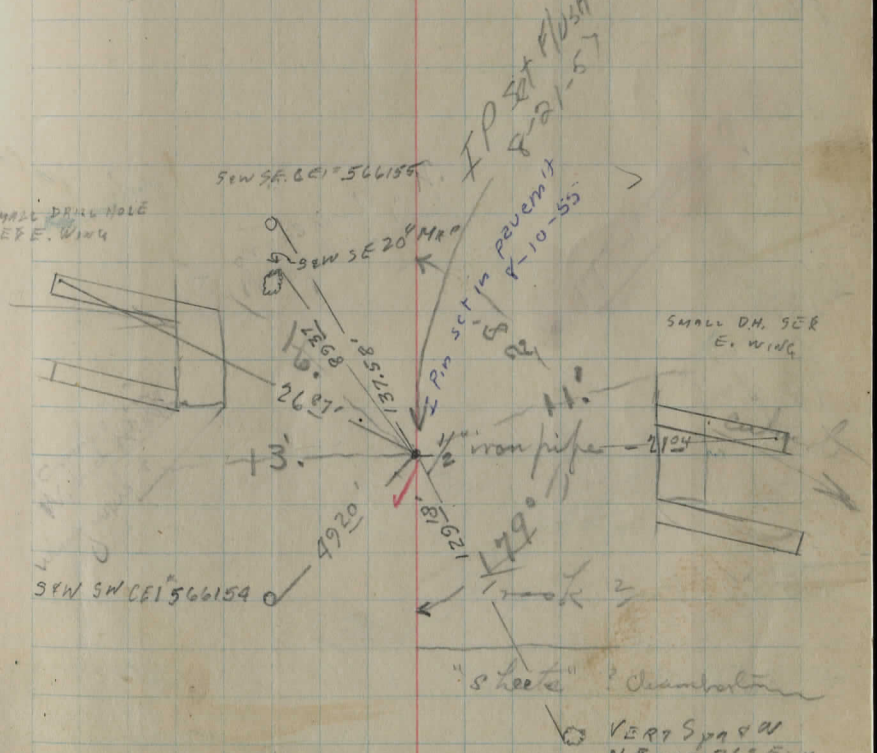
147

+ 09.1 Prop. Line S.

146

145

144



Fiedler & Grant 4/29 – 26

164 wood hub nail in Top. on tang.

163

162

161

160

159

158

157

156

+ 58.8 Prof. Line K. (±)

+ 35.8 Prof Line S. (±)

155

+ 93.8

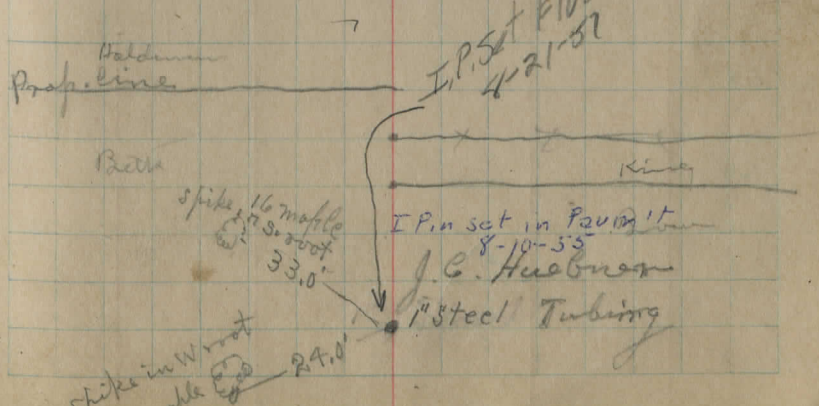
154

+ 0.5 0.1

27.1 x 47'

spike in W.
root 15" maple
7.0

7.0 spike in
N.W. root 18" maple



Tidbr. & Gran 4/29-26

175

174

+07. Pipe sluice

+02. Iron pipe and stones at Lot Corner int & on

173

172

171

170

169

168

167

166

165

Tang. Prof Line

25'

Edge of fence post

88.0

12" Elm

2,267 miles
1 193
3,460

182+70.7
119+23
62 987 ft. = 1.193 mi Lewis Road to old State Road

62987 East of Lewis road to int with old state road

[3.46 mi =

+70.7 Int. ± Old State Road 18,270.7 ft. =

182

181

180

179

178

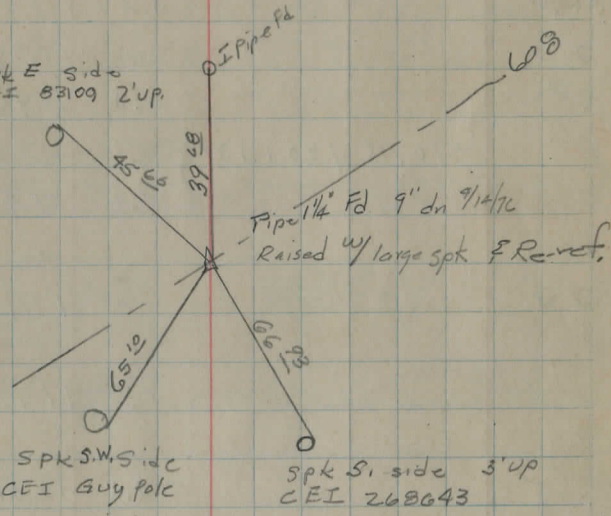
177

176

68+98.83 / 1.2 s-mi-(1.12 ft

8-2 80
1 3 18 8
1 0 8-60
2 6 2 8 8
2 6 4 0 0
-1.12

3.46 Total 43
1 25 Chas
2,21 Hamm



April 30th — 1926 Fudler-Grau & K. Timmer
9:30 Am Cloudy

Sta	+	HI	−	Elev.
114+48	3.24	1190.65		1187.41
			6.80	1183.85
120			4.00	1186.7
Pipe outlet			3.20	1187.5
121			2.1	1188.6
T P			−0.0	1190.65
	+10.48	1201.13		
122			9.9	1191.2
123			6.6	1194.5
124			3.4	1197.7
T.P.			−0.0	1201.13
	+11.95	1213.08		
125			11.2	1201.9
126			7.5	1205.6
127			3.6	1209.5
T P			−0.0	1213.08
	+11.37	1224.45		

37.04 30.0

Long Road 2+ to 7+ 6.8

2 R. 44

R.M. on N root large Elm - spike - water level in Jamb Rt 117

−0.8 −1.0 =1.3 −0.2 +1.0 +1.4 +0.7 +2.5

4.5 5.0 5.3 4.2 3.0 2.6 3.3 1.5

2.5 X 17 16.5 13.0 9 4 0 14 2.8.5 30 35

1185.55 FL 5.1 13.0 FL 1186.40

8 2 4.25 19 2 Long

1.8 1.7 3.1 2.4 1.9 2.2 2.8 1.8 0.3 −0.5

25 18 14.5 11 5 2 1 6 7 9 16 25

+0.3 +1.4 −1.0 −0.3 +0.2 −0.1 −0.7 +0.3 +1.8 − +2.6

+0.3 +0.4 −1.2 −0.4 +0.2

9.6 8.5 11.1 10.3 9.9 10.1 11.3 9.5 9.3 6.5 5.8

25 17 14×15 12 5 9 9 5 4.5 X 6 7 13 17 25

5.8 5.6 8.1 7.2 6.8 6 6 3 8.6 6.0 5.7 4.1 2.9

25 16 12 10 4 6 3 5 X 7 9 12 16 25

3.2 3.6 4.8 4.0 3.2 8 4 3.7 5.3 2.7 1.6 0.0

25 14.5 13 11 4 4X6 9 19 25

9.2 9.6 12.8 11.7 11.2 11.2 11.5 13.5 11.0 9.7 9.0

25 16 12X13 11 4 5 7X8 11 14 25

7.2 6.8 8.7 8.1 7.4 7.5 7.9 9.2 6.7 5.7 5.0

25 14 13X11.5 10.6 4 7 9 12 14.5 25

1.8 2.1 5.1 4.3 3.6 3.6 4.0 5.3 2.2 1.0

25 14.5 12X10.5 9 3.0 8 9X10 13.5 25

Fiddler Grade Time 4/30-26

Sta.	+	H.I.	−	Elev.
128		1224.45	10.1	1214.0
129			6.0	1218.5
130			2.8	1221.7
B.M.			−2.5-0	1221.95
T.P.			−0.0	1224.45
	+11.30	1235.75		
131			11.30	1224.5
132			8.2	1227.6
133			4.5	1231.3
T.P.			−0.0	1235.75
	+9.73	1245.48		
134			8.8	1236.7
135			6.7	1238.8
136			6.2	1239.3
137			4.7	1240.8
	21.03		0.0	

L C R

11.0 / 2.5 — 9.0 / 12 — 12.1 / 8×9 — 16.1 / 7 — 10 — 10.9 / 8 — 12.1 / 9×10 — 9.3 / 15 — 7.4 / 20 — 6.5 / 25

6.3 / 25 — 4.9 / 10.5 — 7.7 / 7×8 — 5.5 / 6.8 — 6 — 6.7 / 6 — 7.6 / 7.5 — 8.5 — 2.8 / 15 — 1.4 / 25

3.5 / 25 — 2.3 / 8 — 3.9 / 6×7 — 3.2 / 6 — 2 — 8 — 2.2 / 5 — 4.0 / 9×11 — 1.4 / 14.5 — 0.9 / 20

drove horizontal spike in S. side of 20" Elm left of Sta 129+75, about 2.5' [illegible]

11.5 / 25 — 10.3 / 8 — 12.5 / 6.5 — 11.7 / 8×8 — 11 — 3 — 11.7 / 9 — 12.5 / 10×11 — 11.0 / 13 — 9.8 / 25

7.2 / 25 — 7.5 / 10 — 9.4 / 7×8 — 8.9 / 6 — 8 — 2 — 8.8 / 8.5 — 9.2 / 10 — 7.6 / 11.5 — 6.6 / 17 — 6.6 / 25

2.2 / 25 — 2.6 / 12 — 5.7 / 8×9 — 5.1 / 6 — 4.5 — 5.1 / 6.5 — 6.0 / 8 — 8.1 / 11 — 1.7 / 25

6.7 / 25 — 8.7 / 11.5 — 9.6 / 9 — 8.8 — 8.5 / 7.0 — 10. / 8 — 7.5 / 10.5 — 6.3 / 25

7.0 / 25 — 7.7 / 20 — 7.5 / 9 — 8.0 / 8.5 — 6 — 7 — 7.5 / 9.0 — 8.1 / 10. — 7.3 / 11 — 7.1 / 26.5

6.2 / 25 — 7.0 / 19 — 6.8 / 10 — 7.1 / 9.5 — 6 — 2 — 6.9 / 8 — 7.5 / 9 — 6.7 / 10.5 — 6.3 / 25

3.5 / 25 — 4.5 / 19 — 4.7 / 11.5 — 5.6 / 10. — 5.1 / 9 — 4.7 — 5.3 / C — 5.8 / 7.5 — 4.9 / 9 — 4.4 / 25

Fadler, Grau & Timond — 4/30-1926

	+R.	H.I. — R.	Elev.
137 + 40		1245.48 — 4.0	1241.5
138		5.1	1240.4
139		5.9	1239.6
140		9.0	1236.5
141		10.6	1234.9
T.P.		-10.77	1234.71
	+2.57	1237.28	
141 + 30		2.8	1234.5
142		3.1	1234.2
+ 45	drain pipe + plank	17 ft hing 3.1	1234.2
143		2.8	1234.5
+ 50		2.6	1234.7
144		4.5	1232.8
145		7.4	1229.9
	2.57	10.77	

L — C — R

2.6 / 2.5	4.1 / 12.5	5.0 / 11	4.6 / 9	3.8 / 2.0	40	4.8 / 5.5	5.2 / 7	4.5 / 8	4.1 / 2.5	
3.4 / 2.5	4.9 / 12	5.9 / 11.5	4.9 / 2	5.1		5.9 / 6	5.1 / 9	4.5 / 19	4.0 / 2.5	
4.8 / 2.5	5.4 / 2.1	5.8 / 12.5	6.7 / 12	6.1 / 10	5.5 / 3	59	6.2 / 3	6.8 / 4.5	6.1 / 5.5	6.3 / 2.0	6.0 / 2.5
6.9 / 2.5	8.1 / 14.5	9.9 / 12.0	9.3 / 11	8.6 / 4.5	90	9.3 / 3	9.6 / 4	8.2 / 5	7.2 / 14.5	7.1 / 2.5	
11.1 / 2.5	10.9 / 14	11.7 / 13	11.3 / 12	10.3 / 8	106	11.0 / 4	11.7 / 6	10.7 / 7	9.6 / 16	9.7 / 2.5	
3.0 / 2.5	3.3 / 14	3.7 / 13.5	2.9 / 11.5	2	8	3.3 / 6.5	4.0 / 7	3.1 / 9.5	0.3 / 15.5	0.4 / 25	
3.6 / 2.5	3.5 / 14	4.0 / 13	3.5 / 11.5	2.9 / 4	3.1	3.6 / 5	4.4 / 6.7	3.8 / 8	4.9 / 2.5		
3.4 / 2.5	3.5 / 15	4.3 / 12	3.7 / 11	3	1	3.7 / 5	4.9 / 5.5	4.6 / 16	7.5 / 7.5	impasse	
2.9 / 2.5	2.7 / 21	3.1 / 20	2.4 / 18	2.7 / 4	28	3.3 / 5.5	4.1 / 7	3.6 / 8	4.4 / 2.1	5.0 / 2.5	
1.8 / 2.5	1.9 / 19	3.0 / 15	2.7 / 14	2.4 / 3	26	3.3 / 5.5	4.0 / 8.5	3.5 / 10.5	3.1 / 14	2.0 / 16	2.5 / 2.5
2.5 / 2.5	3.4 / 15	5.3 / 7.5	4.8 / 1.0	45	5.3 / 7.5	6 / 9	5.1 / 10.5	5.0 / 22	5.7 / 2.5		
4.6 / 2.5	6.5 / 14.5	8.9 / 11.5	8 / 9.5	7.5 / 6	74	8 / 8	8.7 / 9.5	11	8.3 / 12	9.6 / 21	10.3 / 2.5	

G-G.&T. 4/30-1926

	+ R.	H	− R.	Elev.
		1237.25		
146			9.0	1228.3
147			9.5	1227.8
B.M. Roiving	+11.83	1241.21	−7.90	1229.38
			11.80	1229.4
& cub.			13.00	1228.2
148			14.0	1227.2
149			12.7	1228.5
+ 50			11.2	1230.0
150			9.5	1231.7
151			6.1	1235.1
152			2.6	1238.6
T.P. 1	+12.36	1253.57	−0.0	1241.2
153			10.1	1243.5
154			4.9	1248.7
	24.19		0.90	

1141.2 = summit on W hill (124)

Culvert # 3 X5 X18

L.							R.				
7.7 / 25	8.6 / 20	9.9 / 13.5	10.1 / 12.	9.4 / 9.5	9	0	9.3 / 7	10.5 / 10×11	10 / 12	11.3 / 25	
8.3 / 25	9.7 / 20	10.1 / 18	10.8 / 11×12	10.1 / 10	9.5 / 7	9	10.2 / 6	11.5 / 10.5	10.5 / 11	10.4 / 20	10.1 / 25
+ = Rd. ft. on E. end of S. abutment on Culvert over "Cutts" Creek											
− 5 ft. from B.M. to F.L.S. on a Culvert on ℄ 9. L. × 9. R.											
N. parapet, 1.5 to flow line.											
						13					
14.4 / 25	15.2 / 18	14.5 / 9.			14	0	14.2 / 8	15.8 / 12.	14.9 / 16.0	15.2 / 25	
14.4 / 25	13.9 / 11	12.9 / 9			12	7	12.7 / 5	14.1 / 10	14.6 / 25		
12.4 / 25	11.8 / 17	12.3 / 14.5	11.4 / 11		11	20	11.4 / 5	12.7 / 9	12.1 / 10	12.8 / 25	
7.6 / 25	9.0 / 17	10.4 / 15.5	9.8 / 13.5	9.3 / 5	9	5	9.7 / 4	10.3 / 5.5	8.4 / 9	7.3 / 13	7.2 / 25
4.5 / 25	5.5 / 18	6.9 / 15×16	6.3 / 14	5.7 / 7	6	1	6.3 / 2	6.4 / 5×4	5.4 / 5.5	4.2 / 9	3.7 / 25
30 × 0.0 / 25	1.4 / 16	3.5 / 13.	2.9 / 11.5	2.3 / 5	2	6	2.8 / 2.	3.2 / 4.	1.0 / 6	0.0 / 8 × 10	−0.8 / 25
25 + 30 7.4 / 30	9.4 / 13	11.3 / 11.	10.6 / 9.5	9.7 / 4	10	1	10.8 / 14×5	9.2 / 6.5	8.1 / 9.	7.8 / 25	
2.1 / 25	3.1 / 17	4.1 / 13.	5.8. / 11×12	5.1 / 10	4.6 / 4	4	9	5.6 / 4.5	3.9 / 6.	3.2 / 8	2.9 / 17	3.4 / 25

= 0.8 below bot. of road

T. G. + T. 4/30 — 1826

Sta	+ R.	H.I.	− Rod	Elev.
		1253.57		
15-5			2.2	1251.4
15-6			1.0	1252.6
15-5+85			0.5	1253.1
15-6 +50			5.7	1247.9
T.P.			−6.13	1247.44
	+2.97	1250.41		
15-7			5.1	1245.3
+93	Stone Post on cut		6.6	1243.8
15-8			6.9	1243.5
15-9			6.5	1243.9
160			5.3	1245.1
161			2.8	1247.6
160+93				
BM 27' R. of Sta.			−1.52	1248.89
T.P.			−0.0	1250.41
	2.97		6.13	

L R P

1.3 1.9 2.1 2.6 2.0 2.6 2.2 1.8
25+30 19. 13 12. 3. R 2 5. 8 25

2.0 0.0 1.4 1.5 1.1 0.5 1.8
25 12. 10.5 9 1.0 10 14 25

1.6 0.0 1.3 1.0 1.0 0.4 1.0
1 25 12 10 9 0.5 10 14 25

10.5 5.2 4.3 5.6 5.8 5.7 0.3 1.5
25 12 5. 3. 5 9 10 12 20 25

9.2 8.3 7.5 5.1 5.2 5.9 5.2 4.5 3.8
25 21 15 2.0 5 1 13 14 15.5 22 25

1239.6 1239.5
12.0 10.6 10.8 5.8 6.6 6.8 5.7 11.0 9.4 8.5
100 6.0 5.2 5.2 3 6 6 10 11.7 11.7 20 25

8.7 8.6 9.1 8.5 7.7 7.0 6.9 10.3 9.2 8.2
25 11.5 10 8.5 5 4. 6 9 13. 19 25

7.1 6.8 7.2 6.6 6.2 6.8 7.2 6.4 6.8
25 6 8.5 4 6.5 4 11 12.5 13.5 25

5.4 5.0 6.1 5.5 4.8 5.5 6.1 5.1 5.7
25 5. 3 4 4 2 5 3 8.5 12.5 17 15.5 20

0.5 1.3 2.6 3.7 2.3 3.0 3.7 2.7 1.7 1.6
25 12 9 6 4 2 5 5 10 14 15 18 25

20" maple. Spike in knot

F.G. & T. 4/30-1926

Sta	+Rod	H.I.	−Rod	Elev.
				1251.41
	+11.60	1262.01		
162			10.6	1251.4
163			6.0	1256.0
+70			1.6	1260.4
T.P.			−0.0	1262.01
	+10.46	1272.47		
164			11.1	1261.4
165			9.7	1262.8
166			8.5	1264.0
167			6.7	1265.8
168			3.7	1268.8
169			1.5	1271.0
T.P.			−0.0	1272.47
	+8.14	1280.61		
170			8.1	1272.5
	30.20		0.0	

L & R

25	7.3 / 25	7.8 / 11	12.2 / 4.8	11.0 / 2.	10	60	10.6 / 5.	11.2 / 10.	11.5 / 11.5	10.1 / 13	7.9 / 17.	7.7 / 25
	2.0 / 11	2.0 / 11	3.0 / 7.5	2.7 / 8		60	5.7 / 5.	6.3 / 11	7.2 / 12	7 / 13	7 / 17.	1.9 / 16
	−1.9 / 25	−1.0 / 8	0.0 / 4	2.6 / 2	1.6		1.0 / 7	1.6 / 13.	2.5 / 14	8/6	−0.4 / 25	
25	9.2 / 22	10.3 / 4	12.2 / 2.	11	1		10.4 / 7.	11.3 / 15	11.8 / 16	10.6 / 17	10.3 / 25	
	10.5 / 25	9.6 / 7	10.5 / 2		9.7		9.2 / 6	9.7 / 13	10.3 / 14.5	9.5 / 15	10.1 / 15	
	7.9 / 25	8.6 / 5	9.5 / 4.	8.6 / 2	8.5		8.2 / 5	8.7 / 17	9.4 / 26	8.8 / 17	9.0 / 14	
25	3.6 / 25	3.4 / 15	4.1 / 9	5.4 / 6.	7.4 / 4	6.5 / 3	6.9	6.4 / 7	7.2 / 16	7.9 / 11.5	8.1 / 16	3.8 / 25
	2.2 / 25	3.3 / 6.	4.4 / 4	4.0 / 3.	3.7		3.5 / 5	4.8 / 11	5.0 / 13	2.5 / 17	2.3 / 25	
	1.5 / 25	1.4 / 7	2.3 / 5	1.8 / 4	1.5		1.5 / 8.5	2.1 / 10.	2.5 / 12.	1.3 / 14	0.6 / 25	
	8.0 / 25	7.6 / 7	8.6 / 6	8	1		8.4 / 7	8.7 / 12	7.2 / 14	6.8 / 25		

F. G. + T. 4/30-1926

	+R	HI	−R.I	Elev.
		1280.61 ✓		
171			5.2	1275.4 ✓
172			4.2	1276.4 ✓
173			4.7	1275.9 ✓
173+07	Culvert Life		4.9	1275.9 ✓
174			4.4	1276.2 ✓
175			3.7	1276.9 ✓
176			2.6	1278.0 ✓
4:45 P.M. quit				
B.M. Fiedler + E. Keeney 177	20" Cherry Tree +14.58	✓	−0.80	1279.81 ✓ 1279.7
178			9.3	1282.1 ✓
179			5.1	1286.3 ✓
+45			3.4	1288.0 ✓
180			3.1	1288.3 ✓

L & R

4.8/25 4.4/9 6.1/9 5.6/6 5 2 5.8/8 6.4/10.5 4.4/13 3.8/25

4.0/25 4.5/14 5.8/11 5.1/9 4 2 4.8/9 5.5/10 4.5/11 3.6/25

5.7/25 5.4/15 6.0/13 5.2/11 4.5/2 4 7 5.2/6 5.9/9 4.8/9 4.0/25

1274.1 1275.3 1274.4

10.00/100 2.6/50 6.5/10.4 5.3/10.4 4 7 5.3/6.2 6.2/6.2

6.0/25 5.5/17 4.8/16 5.4/14 4.7/12 4.1/5 4 4 4.9/21 5.1/4.5 4.6/6 3.5/25

4.8/25 4.6/19 4.0/16 4.6/15 4.0/13 3.7/5 3 7 4.4/5 3.8/6 2.4/25

2.6/25 3.0/19 2.5/15 3.3/18 2.9/17 2.2/12 2 6 3.2/6 2.6/7 0.7/25

175+47, X 18'6 Rd ℄ = 8 like in Needs drove horizontal

10.5/16 11.0/14 12.5/12 12.0/10 11.4/3 11.7 12.2/5 11.7/6 11.4/14 11.0/25

9 3

6.6/25 6.9/15 7.8/12 8.9/11 9.2/4 9.3 9.9/5 8.3/7 8.2/18 X 25

1.9/25 2.4/19 3.3/15 6.1/10 4.9/3 5.1 5.6/5 6.0/6 3.7/8 3.9/8 4.4/22 4.9/25

1.0/25 1.4/19 2.9/15 4.3/12 3.6/12 3.1/3.5 3.4 4.1/6 3.4/9 3.5/13 4.7/20 X 25

1.2/25 1.5/20 1.9/16 4.1/13 3.4/11 2.9/3 3.1 4.0/7 3.2/8 3.4/17 5.0/25

Fiedler + E. Keeney 5 — ± X

	+ Rod	F.S.	− Rod	Elev.
181		1291.39 ✓	3.7	1287.7 ✓
182			3.2	1288.2 ✓
+50			2.5	1288.9 ✓
+70.7 = int. × Ter. = 20.8 Rd			2.2	1289.2 ✓
180+70	80" cor. × vit. fix. above line taken water from W. side "Old State Road"		3.6	1287.8
T.C.			1.68	1289.71
	+12.92			
		1302.43 ✓		
BM at 160+05 Old State Rd			0.74	1301.69 ✓
" " "				1301.87
				Error +0.18

182 + 70.7 = 18-6 + 59.5 of Old State Rd intersection

Old State Road BM 1301.87

1301.92 = x sea level

2.2 / 25	2.0 / 22	2.5 / 19	4.1 / 17	2.9 / 14	3.3 / 5	3	7	4.2 / 2	3.8 / 7	4.4 / 13
5.0 / 14	6.1 / 25									
25 ×	1.3 / 23	1.5 / 20	2.7 / 17	2.1 / 15	2.7 / 6	3	2	3.5 / 9	4.1 / 11	4.5 / 25
	1.6 / 25	1.8 / 20	2.0 / 12	2.4 / 8	2	5	2.5 / 5	2.8 / 10	2.2 / 12	2.4 / 25
					2.2					
	4.3 / 17 F.L.		3.6 / 14		3	6	3.9 / 4	5.0 / F.L.	6.8 / 35	8.7 / 50
10.5 / 70										

W. root of walnut front of Greenwood house 160 + 05 Rt. of

B.M.	11.13	1290.94		1279.81	
179					1287.20
178					1283.60
B.M	10.06	1258.95		1248.89	
162				1253.00	5.95
	10.86	1265.80	4.01	1254.94	
163				1257.00	8.80
163+70				1259.80	6.00
164				1261.00	4.80
B.M	7.16	1256.05		1248.89	
156				1252.00	4.05
155				1250.75	5.30
154				1249.50	6.55
153				1245.00	11.05
B.M	7.73	1237.11		1229.38	
144				1233.50	3.61
143				1235.20	1.91
	9.80	1244.43	2.48	1234.63	
139				1240.00	4.43
138				1241.20	3.23
137				1241.50	2.93

May. 5, 1927, Marks-Graa-Snyder

52

Spike N. side 20" Cherry, R. 175+47

	C 2.1	C 0.2
	22.0	20.0
3.74	C 1.0	0.0
7.34	21.0	19.0

Spike, W. Root 20" Maple, R. 160+93

C 1.9	C 1.4
25.0	21.5
C 3.4	C 3.3
23.5	25.0
C 3.6	C 2.5
25.0	20.0
C 2.5	C 1.3
22.0	21.0

Spike, W. Root 20" Maple, R. 160+93

C 3.3	C 2.6
24.0	23.0
C 1.5	C 1.1
21.0	21.0
C 1.7	C 1.1
21.0	21.0
C 0.4	C 0.7
19.0	21.0

Cross on E, End 5. Abutment, Cutt's Creek,

C 0.8	F 1.1
20.0	18.0
F 0.6	F 2.1
19.5	17.5
0.0	F 0.7
19.0	18.5
0.0	0.0
19.5	19.5
F 0.4	F 0.3
19.5	19.0

	8.19	1242.40		1234.21	
	9.56	1248.11	3.85	1238.55	
72					1241.73
71+50					1237.57
B.M.	8.19	1242.40		1234.21	
71+00					1232.95
B.M.	2.58	1236.79		1234.21	
70+50					1228.00
	0.69	1228.47	9.01	1227.78	
70+00					1223.25
	0.92	1217.20	12.19	1216.28	
69					1213.55
	0.00	1205.82	11.38	1205.82	
68					1203.85
67					1196.18

June 9, 1927, Marks, D. Parks, Hassel

53

B.M. Left 70+75

6.38	C 1.9 / 22.0	C 1.9 / 21.5
10.54	C 3.8 / 24.0	C 2.6 / 23.5
9.45	C 4.4 / 25.5	C 5.6 / 28.5
8.79	C 2.6 / 24.0	C 6.4 / 29.5
5.22	0.0 / 19.0	C 4.5 / 26.0

69+20 Spring, Drain to North

3.65	F 2.3 / 17.0	F 2.3 / 17.8
1.97	F 2.4 / 17.0	F 0.8 / 17.0
9.72	F 1.8 / 17.5	F 0.8 / 17.5

June 16, 1927 Parks, D. Parks, Hassel

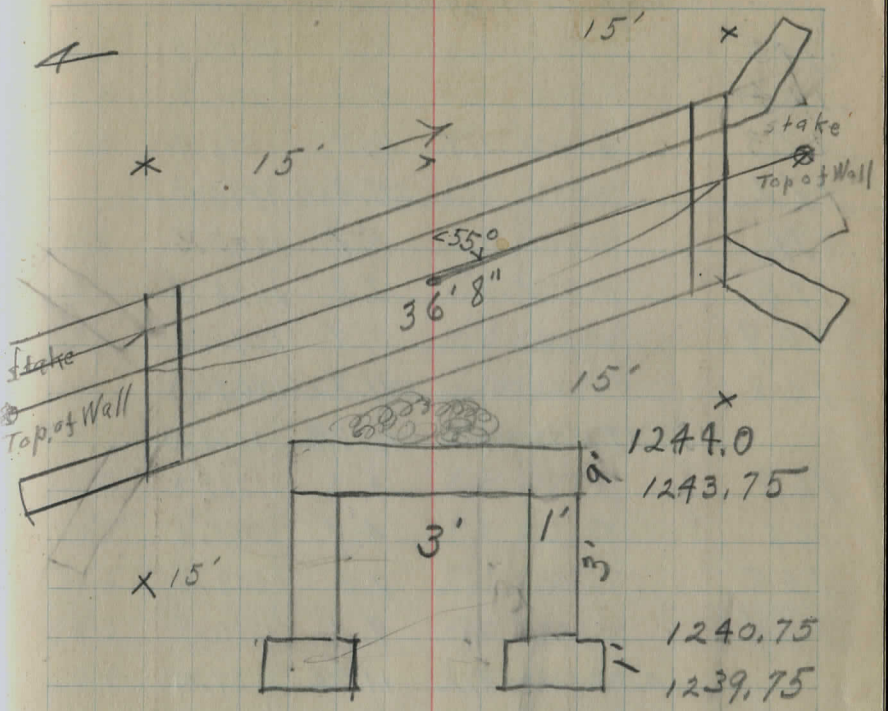
54

Culvert

158+10 ±

R. 160+93

B.M	0.16	1249.05		1248.89
			5.30	1243.75
	0.24	1249.13		1248.89
			5.38	1243.75



Profile of Sub Grade

R. - 175+47

	+	H.I.	−	El.
B.M	10.69	1290.50		1279.81
182+70.7			1.3	1289.2
182			1.8	1288.7
181			2.2	1288.3
180			2.4	1288.1
179			4.1	1286.4
178			7.2	1283.3
177			10.0	1280.5
176			12.0	1278.5
B.M			10.69	1279.81

Sta.	+	H.I.	−	El.	
	1.48	1281.29		1279.81	
175			3.8	1277.5	
174			4.4	1276.9	
173			4.9	1276.4	
172			5.3	1276.0	
171			5.7	1275.6	
170			7.8	1273.5	
169			9.8	1271.5	
168			11.8	1269.5	
	0.97	1270.47	11.79	1269.50	
167			3.3	1267.2	
166			4.9	1265.6	
165			7.0	1263.5	
164			9.7	1260.8	
	0.70	1259.71	11.46	1259.01	
163			2.1	1257.6	
162			6.8	1252.9	
161			11.2	1248.5	
160+93-R. B.M.			10.87	1248.84	
B.M.	4.01	1252.90		1248.89	(record)
160			7.3	1245.6	
159			8.7	1244.2	
158			9.1	1243.8	
157			5.4	1247.5	
156+35			2.4	1250.5	
156			1.7	1251.2	

Sta.	+	H.I.	−	El.
		1252.90		
155			2.6	1250,3
154			4.2	1248,7
153			8.3	1244.6
	0.37	1244.52	8.75	1244.15
152			3.9	1240,62
151			8.2	1236,32
150			11.5	1233,02
	2.85	1235 .83	11.54	1232.98
149			7.1	1228,73
148			8.4	1227,43
147			8.0	1227,83
146			7.6	1228,23
145			5.6	1230,23
144			3.1	1232,73
143			1.3	1234,53
	8.45	1242.90	1.38	1234.45
142			8.1	1234,8
141			7.1	1235,8
140			5.3	1237,6
139			3.3	1239,6
138			2.3	1240,6
137			2.3	1240,6
136			2,7	1240,2
	2.08	1242 .06	2.92	1239.98
135			3.5	1238,56

Stg.	+	H.I.	-	El.	
		1242.06			
134			5.9	1236.16	
133			9.7	1232.36	
	1.25	1231.55	11.76	1230.30	
132			3.3	1228.25	
131			6.5	1225.05	
130			9.6	1221.95	
Left 129+70 B.M.			9.56	1221.99	
	1.19	1223.14		1221.95	Record
129			4.5	1218.64	
128			8.8	1214.34	
	0.67	1212.14	11.67	1211.47	
127			2.5	1209.64	
126			6.4	1205.74	
125			10.1	1202.04	
	0.37	1200.34	12.17	1199.97	
124			2.2	1198.14	
123			5.5	1194.84	
122			8.7	1191.64	
121			11.2	1189.14	
	1.01	1190.27	11.08	1189.26	
120			3.4	1186.87	
119			4.6	1185.67	
118			5.1	1185.17	
117			5.6	1185.67	
116			5.0	1185.27	
115			3.4	1186.87	

Stg.	+	H.I.	-	El.	
		1190.27			
Right 114+48 B.M.			2.90	1187.37	
	6.74	1194.15		1187.41	Record
114			6.7	1187.45	
113			6.3	1187.85	
112			5.5	1188.65	
111			5.0	1189.15	
110			4.1	1190.05	
109			3.1	1191.05	
108	11.33	1204.18	1.30	1192.85	
107			10.0	1194.18	
106			8.6	1195.58	
105			7.1	1197.08	
104			5.3	1198.88	
103			2.9	1201.28	
102			0.0	1204.18	
	12.02	1215.24	0.96	1203.22	
101			7.9	1207.34	
100			4.0	1211.24	
	9.86	1224.71	0.39	1214.85	
Right 99+45 B.M.			7.85	1216.86	
B.M.	7.85	1224.66		1216.81	Record
99			8.0	1216.66	
98			2.2	1222.46	
	11.12	1235.76	0.02	1224.64	
97			7.5	1228.26	

Sta.	+	H.I. 1235.76	−	El.	
96	11.56	1246.72	0.60	1235.16	
95			4.8	1241.92	
	11.73	1257.38	1.06	1245.66	
94			8.8	1248.59	
93			3.5	1253.89	
	10.71	1267.00	1.10	1256.29	
92			8.7	1258.30	
91			4.8	1262.20	
	11.78	1276.28	2.50	1264.50	
90			9.4	1266.88	
89			5.4	1270.88	
L. 88+85 B.M			1.92	1274.36	(1274.39)
88			2.6	1273.68	
87			1.0	1275.28	
86			1.2	1275.08	
85			1.2	1275.08	
	4.05	1278.39	1.94	1274.34	
84			4.0	1274.39	
83			4.5	1273.89	
82			5.3	1273.09	
81			5.4	1272.99	
80			5.9	1272.49	
79			7.2	1271.11	
78			8.9	1269.49	
	2.05	1271.01	9.43	1268.96	
77+70			2.1	1268.91	

Sta.	+	H.I. 1271.01	−	El.	
77			5.0	1266.01	
76			9.8	1261.21	
	0.22	1259.05	12.18	1258.83	
75			2.3	1256.75	
74			6.8	1252.25	
73			11.1	1247.95	
	0.01	1247.63	11.43	1247.62	
72			5.9	1241.73	
71			~~11.9~~	~~1235.73~~	
	4.65	1240.43	11.85	1235.78	
L. 70+75 B.M.			6.30	1234.13	Record. 1234.21

	Grade Rod	Rod Top of Stakes	Cut
4+00	9.7	7.2	C 2.5
3+00	8.9	6.9	2.0
2+00	8.1	5.1	C 3.0
1+00	7.3	4.8	C 2.5
10.6 Left of Sta 118+91, ℄ Sta. of Rd. 0+00	6.5	4.5	C 2.0
5+00	10.5	9.0	C 1.5

June 20, 1927. Marks, D. Parks, Hassel

58

8.1/6 8.2/0 8.1/21 8.1/41 7.3/66 7.3/75 7.3/89

4.7/29 7.3/24 6.7/18 7.1/5 7.3/0 7.1/5 7.1/22 7.3/44 6.7/62 7.2/71 6.3/105

5.2/43 6.0/37 6.2/21 5.8/0 5.9/5 5.9/13 5.7/41 5.3/65 5.6/92 5.7/123 3.2/130

3.7/40 5.7/33 5.6/27 5.9/22 5.4/5 5.3/0 4.6/13 5.5/17 4.8/23 4.5/51 2.4/63

4.5/0 Top of Opening of Culvert at N. End.

10.5/3 Bo

	2.77	1114.44		1111.67	
49					1110.50
48					1105.40
47+50					1102.00
	2.60	1107.40	9.64	1104.80	
47					1097.00
46+50					1092.00
	1.32	1097.50	11.22	1096.18	
46	1.14	1088.14	10.50	1087.00	1087.00
45+50					1082.00
45					1077.00
	0.68	1077.32	11.50	1076.64	
44+50					1072.00
44					1067.57
	4.52	1069.84	12.00	1065.32	
			8.16	1061.68	

B. M. Right 48+91

3.94	C 2.8 / 23.0	C 0.4 / 20.0
9.04	C 4.4 / 26.0	C 1.7 / 20.5
12.44	C 7.4 / 31.0	C 1.0 / 24.5
10.40	C 9.9 / 36.0	C 5.2 / 28.5
15.40	C 13.0 / 38.0	C 4.8 / 28.0
10.50	C 12.1 / 35.0	0.0 / 17.0
6.14	0.0 / 17.5	F 2.1 / 17.5
11.14	F 4.2 / 20.0 stake nailed on Tree	C 3.0 / 24.0
5.32	F 4.9 / 22.0	F 5.2 / 22.0
19.75	F 2.3 / 15.0	F 5.5 / 22.0

(1061.68) Rec, B. M. L, 42+90

June 30, 1927 Marks-D Parks, Hassel

	1.32	1235.53		1234.21	
	0.02	1224.48	11.07	1224.46	
70	~~0.02~~				1223.25
69					1213.55
	0.17	1213.77	10.88	1213.60	
68					1203.85
	0.40	1203.83	10.34	1203.43	
67					1196.10
				1.977	

B. M. L. 70+75

1.25

10.93

9.92

7.73

Profile of Sub-Grade

Stq	+	H.I	−	El.
B.M.	6,40	1163,88		1157.48
1			6,4	1157.48
2			3,3	1160,58
3			2,6	1161,28
4			2,6	1161,28
T.P.	3,53	1164,65	2,76	1161,12
5			3,3	1161,35
6			4,0	1160,65
7			4,9	1159,75
8			5,1	1159,55
9			6,4	1158,25
10			8,3	1156,35
T.P.	0,01	1156,24	8,42	1156,23
11			2,7	1153,54
12			6,3	1149,94
13			9,7	1146,54
14			12,1	1144,14
T.P.	0.88	1145.10	12,02	1144,22
15			2.9	1142.20
16			3.9	1141.20
17			4.4	1140.70
18			4.8	1140.30
19			5.3	1139.80
20			6.8	1138.30
21			10.2	1134.90
			10.64	1134,46

Aug. 4, 1927

Sta	+	HI	−	EI	
T.P	0.47	1134.93	10.64	1134.46	
22			4.4	1130.53	
23			10.1	1124.83	
T.P.	0.25	1125.10	10.08	1124.85	
24			6.9	1118.20	
25			12.7	1112.40	
T.P	0.34	1113.34	12.10	1113.00	
26			7.1	1106.24	
27			13.1	1100.24	
T.P	1.17	1102.78	11.73	1101.61	
28			7.4	1095.38	
29			8.7	1094.08	
30			8.9	1093.88	
T.P.	4.83	1099.18	8.43	1094.35	
B.M.			1.85	1097.33	
B,M	3,21	1100,61		1097,41	Record
31			6,0	1094,61	
32			5,1	1095,51	
33			3,8	1096,81	
34			2,9	1098,71	
35			5,1	1095,51	
T.P.	1.00	1096.49	5,12	1095,49	
36			8,1	1088,39	
TP	1,43	1085,80	12,12	1084,37	
37			4,9	1080,90	

	6.74	1104.15		1097.41	
38					1097.40
	5.40	1107.60	1.95	1102.20	
34					1099.15
34+50					1098.35
35					1096.35
	0.76	1096.41	11.95	1095.65	
35					1096.35
36					1089.00
37					1081.30
	2.65	1100.06		1097.41	
28					1096.50
	9.55	1107.72	1.89	1098.17	
27					1101.00
	10.66	1117.66	0.72	1107.00	
26					1107.00
	9.98	1126.36	1.08	1116.58	
25					1113.00
24					1119.00
			0.49	1125.87	

July 11, 1927 Marks, D. Parks, Hassel

6.75	F. 0.7 / 18.0	C 4.8 / 25.0
8.45	C 5.5 / 26.0	C 1.0 / 21.0
9.25	C 8.4 / 31.5	C 4.7 / 26.0
11.25	C 5.9 / 29.5	—
0.06	—	0.0 / 19.5
7.41	0.0 / 15.0	F 7.6 / 26.0
15.11	C 3.4 / 24.0	F 1.2 / 17.5

July 12, 1927 Marks, D. Parks-Hassel

3.56	0.0 on Tel. Pole	F 2.0 / 17.0		F 1.6 / 18.0
6.72	F 3.3 / 18.0		F 2.8 / 17.0	0.0 on Post
10.66	0.0 / 19.0			C 0.5 / 16.0
4.66	C 2.8 / 22.5			0.0 / 20.0
7.36	C 1.1 / 20.5			0.0 / 19.5

	11.22	1137.09		1125.87	
23					1125.00
22					1131.00
	6.93	1141.57	2.45	1134.64	
21					1136.06
20					1139.00
19					1140.55
	8.82	1166.30		1157.48	
1					1158.60
2					1161.70

12.09	C 3.0 / 22.5	C 1.4 / 21.5
6.09	C 3.6 / 24.5	C 3.5 / 24.5
5.51	C 1.3 / 21.5	C 2.2 / 22.5
2.57	F 0.8 / 18.0	C 1.2 / 20.5
1.02	0.0 / 19.0	C 1.9 / 22.0

B.M. Right 0+14

7.70	C 1.4 / 22.0	C 1.2 / 21.5
4.90	0.0 / 20.0	C 2.0 / 22.0

Profile of Sub-Grade

Sta	+	H.I. 1085.80	−	El	
38			10,7	1075,10	
T.P.	0.04	1075.21	10,63	1075,17	
39			4,8	1070,41	
40			8,4	1066,81	
41			11,3	1063,91	
T.P.	3,83	1067,81	11,23	1063,98	
B.M.			6,15	1061,66	1061.68 Rec.

Sta	+	HI	−	El	
B.M.	4.34	1116.01		1111.67	
49			6.2	1109.8	
50			2.6	1113.4	
T.P	12.24	1127.74	0.30	1115.7	1115.71
51			11.6	1116.3	
52			8.1	1119.8	
53			3.8	1124.1	
T.P	11.36	1138.74	0.56	1127.38	
54			8.2	1130.5	
55			1.6	1137.1	
T.P	11.84	1150.24	0.34	1138.40	
56			7.2	1143.0	
57			1.3	1148.9	
T.P	12.48	1162.46	0.26	1149.98	
58			7.6	1154.9	
59			1.9	1160.6	
T.P	4.59	1166.21	0.84	1161.62	
B.M			0.38	1165.83	Record 1165.82
TP	8.60	1170.22		1161.62	
60			5.9	1164.3	
61			2.2	1168.0	
T.P.	12.04	1181.96	0.30	1169.92	
62			10.7	1171.3	
63			7.8	1174.2	
64			3.5	1178.5	

Sta	+	Hi 1181.96	−	El
T.P.	11.97	1193.41	0.52	1181.44
65			9.3	1184.1
66.			3.6	1189.8
T.P.	12.26	1205.55	0.12	1193.29
67			10.8	1194.7
68			2.9	1202.6
T.P.	12.85	1218.38	0.02	1205.53
69			6.2	1212.2
T.P.	12.12	1230.32	0.18	1218.20
70			7.7	1222.6
70+50			2.2	1228.1
T.P.	12.67	1242.84	0.15	1230.17
B.M.			8.60	1234.24 record 1234.21
71			9.0	1233.8
72			1.6	1241.2
T.P.	11.15	1253.69	0.30	1242.54
73			6.0	1247.7
74			1.0	1252.7

Cutts Road #12
Lewis Rd. Hambden Tp

208.2

27+56.98 P.I.

1. Pin Set

44 2.20

S&W
N. side
10" Soft Maple
4' above Gr.

S. spike E. Side
12" Apple

SEE Pg 70
new ref

23+14.74 P.I.

1. Pin Set

258.80

Spike in
"V" 10" W. Cherry

Spike in
S.E. Side
60" Soft Maple
3' above Gr.

170+55.95 P.I.

Spike in
N. side 12"
W. Cherry

1. Pin Set

187.50

Spike in
"V" S.E. Side
10" Soft Maple

B Spike in "V" SE.
Side 14" W. cherry

18+68.45 P.I.

(14+13.73 Spring Rd 6-3-55)

1. Pin Set

(West Edge of travel)
Gravel 10' wide

56.95'

5 in
26" W. Cherry

5 in S. Root 24" Locust
(P.C.C. Spike)

10+74.68

Fence

3130

Spike in S. Root 24" Locust

0+00 (Hambden Center) Road

Iron Pipe Ed-

C+1.25

64

26+45

26+15 Fence B. P.L.?

24+62.30

13' × 1.9' × 10.1 — 5' × 8' — 12.5 F.L. — 4.5 Gravel or Tip

24' × 2.8' × 9.2' — 16' Span (16 × 9') — 4.7 Tip: #8 Gravel — 149 F.L.

X-Section

Lattice Truss

2-9" channels

± 3"x3" Angle Needle beam

4-Is 4½"x9" x 20-00

See Pg 77 for 1966 work

19+35

24" W. Cherry

Fence B P.L.

19"

Large

17+87 P.L.

Fence A

P.L.

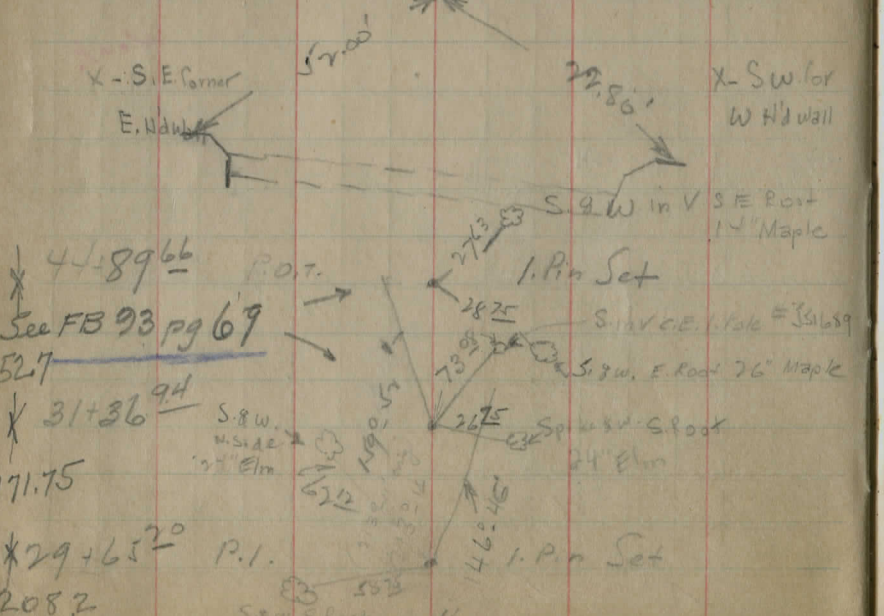
17+67

Fence

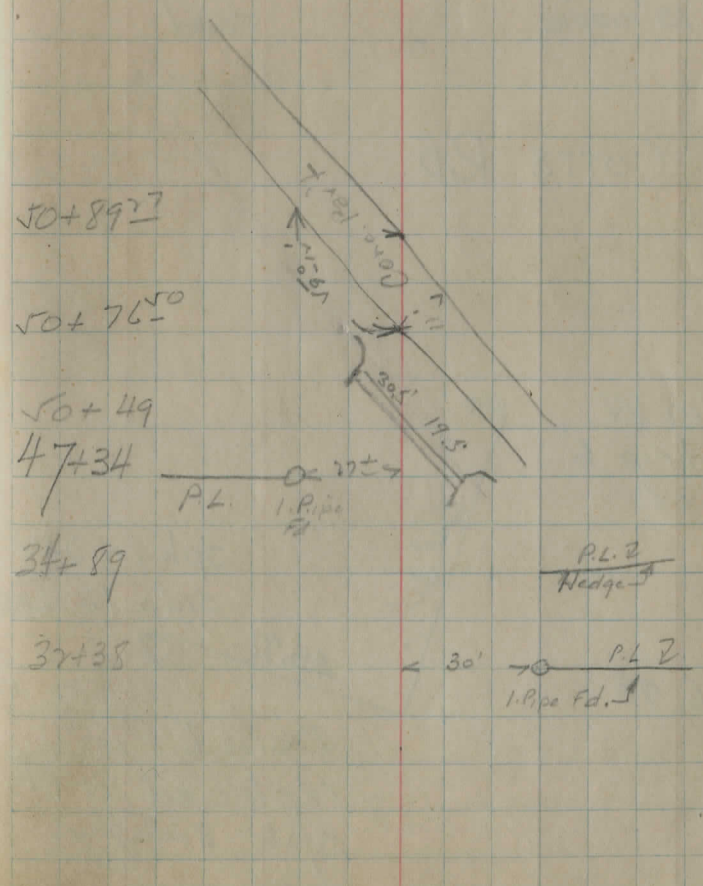
50+76.5
44+89.65
5 86.85

See Pg. 77 for 1966 work

.961 miles
5280 | 5074

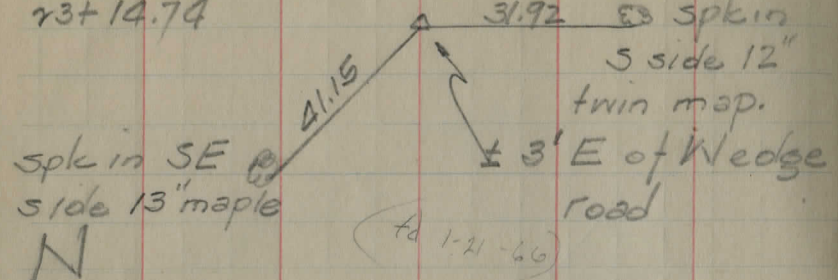


69.

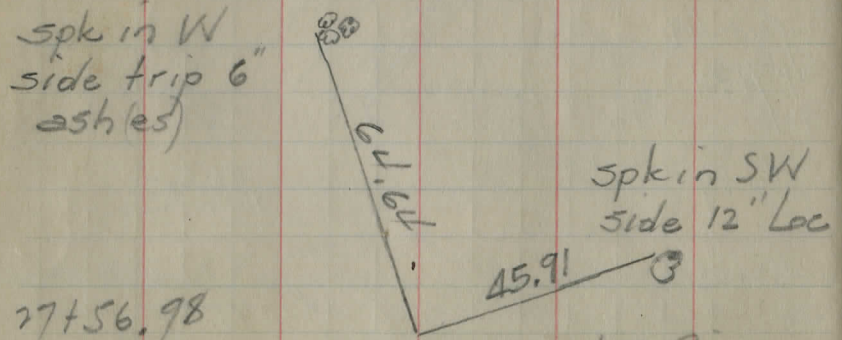


½" I. Pin fd & raised to near flush with ½" I.P. 8-4-54

23+14.74



COTTS RD



27+56.98

Bent I. Pin replaced with spk 8-4-54

(No find 1-21-66)

SUMNER SEE Pg 77 F.B. 89

T.H. 67 ~~Queen~~ Road.

Hopkden Twp.

Notes copied from Fiedlers notes

Sta 0+00 County Line.

Fiedler
Winchell 6/7/33

12+15 Prop. Line

12" Pipe Culv. 8+91

7+10 M

North

Stone Box Culvert
3 x 2 x 20'

2+16 →

30'

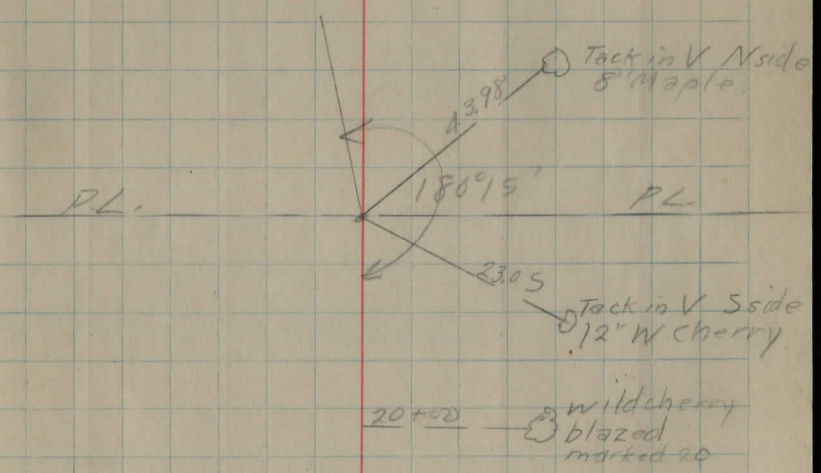
Pipe Rd

N 3°30' E

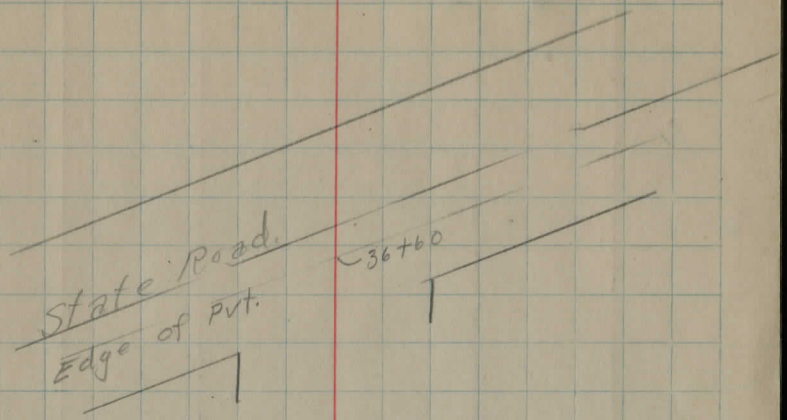
Sta 22+10 Def Lt 0°15'

Pipe Culv. 27+12

Pipe Culv. 23+33



12" Pipe Culv. 13+05



33+93
30'
Pipe on Prop. Line to West

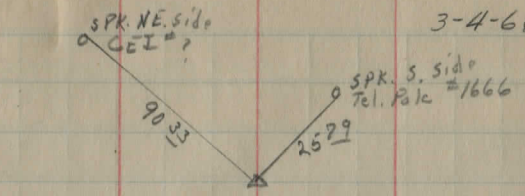
Pipe Culv. 33+55

Pipe Culv. 30+47

H. Patterson
R. Diedrich

Cutts Rd. #72

3-4-66

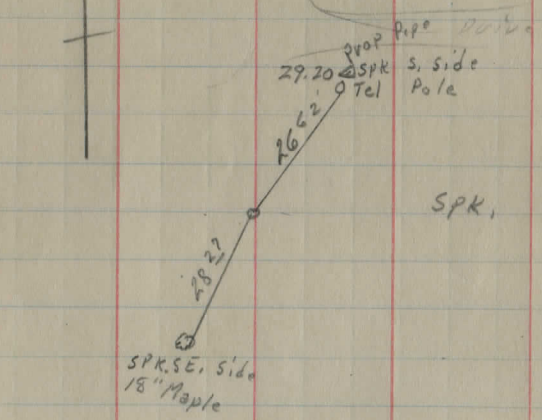


13+36.01

I.P. P.O.T.

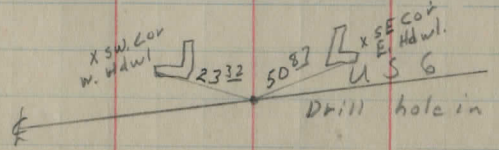
Drive

29.20 Δ Prop Pipe



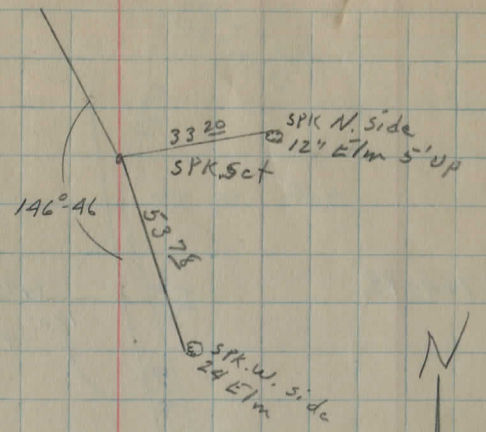
5+86.85

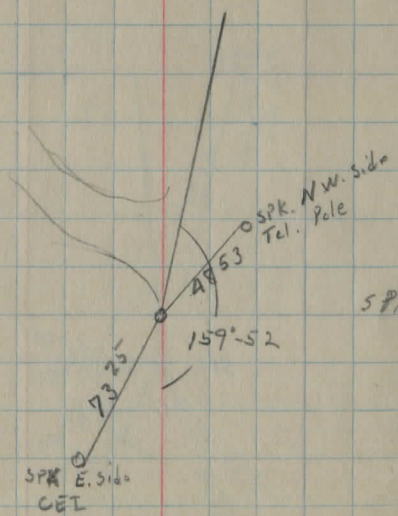
SPK. P.O.T.



0+0

21+11.35





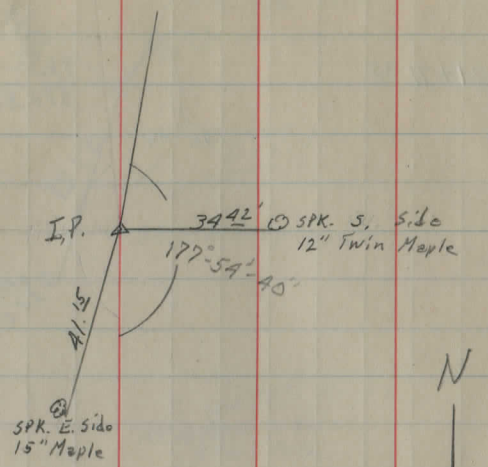
19+39.60

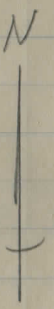
SPK. set

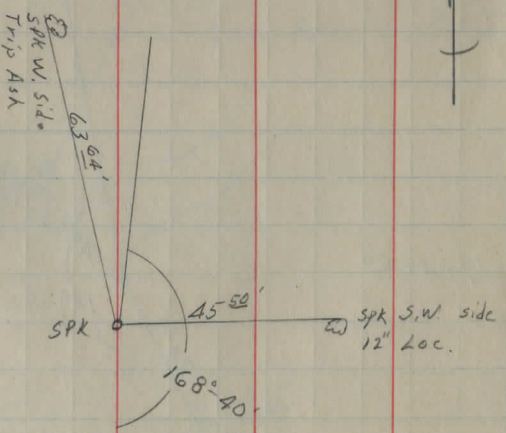
18+33.94

Prop Pipe Δ 30'

27+40 84

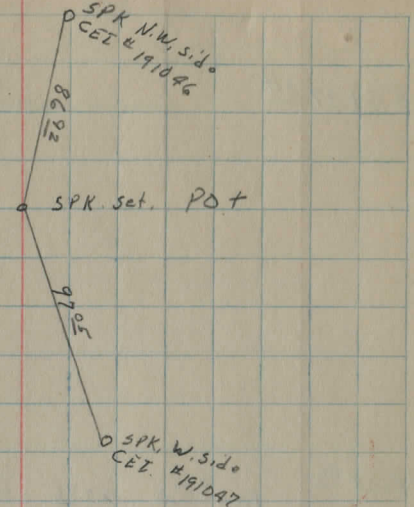


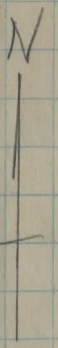




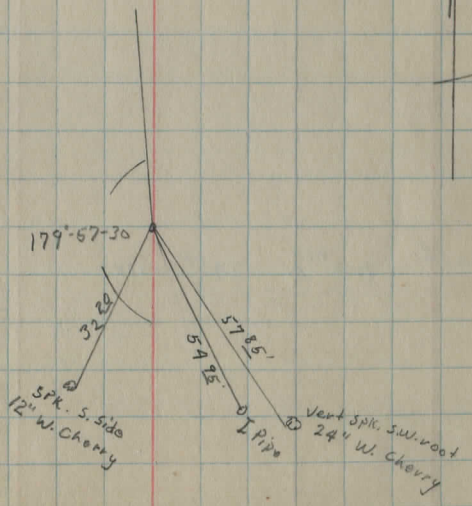
23+19 55

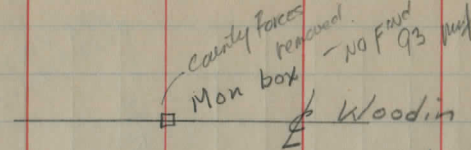
39+46 20



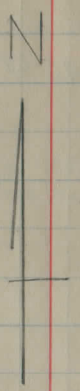


31+61 09





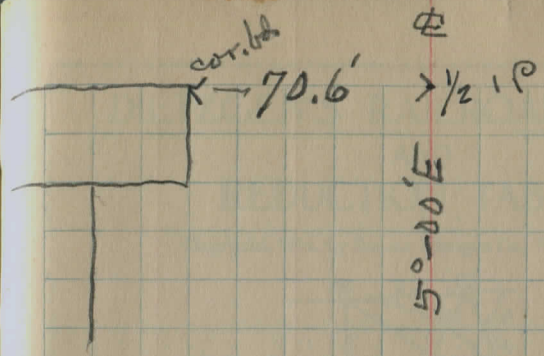
50+29.24



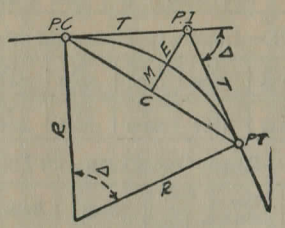
48+08.86 Prop Pipe △ 29.96 ○ SPK

47+49.04 SPK ○ 29.96 △ Prop Pipe

45+80.54 Prop Pipe △ 29.88 ○ SPK


cor. bk
70.6'
℄
½ ip
N 5°-00'-E

DIETZGEN'S RAILROAD CURVE AND REDUCTION TABLES



CURVE FORMULAS

Radius=R=$\frac{50}{\sin. D/2}$ (1) Degree of Curve=D and sin. $\frac{D}{2}=\frac{50}{R}$ (2)

Tangent=T=Rtan$\frac{\Delta}{2}$ (3) Length of Curve=L=100$\frac{\Delta}{D}$ (4)

Middle ordinate=M= R(1—cos. $\frac{\Delta}{2}$) (5) =Rvers $\frac{\Delta}{2}$ (6)

External=E=Ttan$\frac{\Delta}{4}$- (7) =R÷cos.$\frac{\Delta}{2}$–R (8)=Rexsec$\frac{\Delta}{2}$ (9)

Long Chord=C=2 R sin.$\frac{\Delta}{2}$ (10) Δ=Central Angle

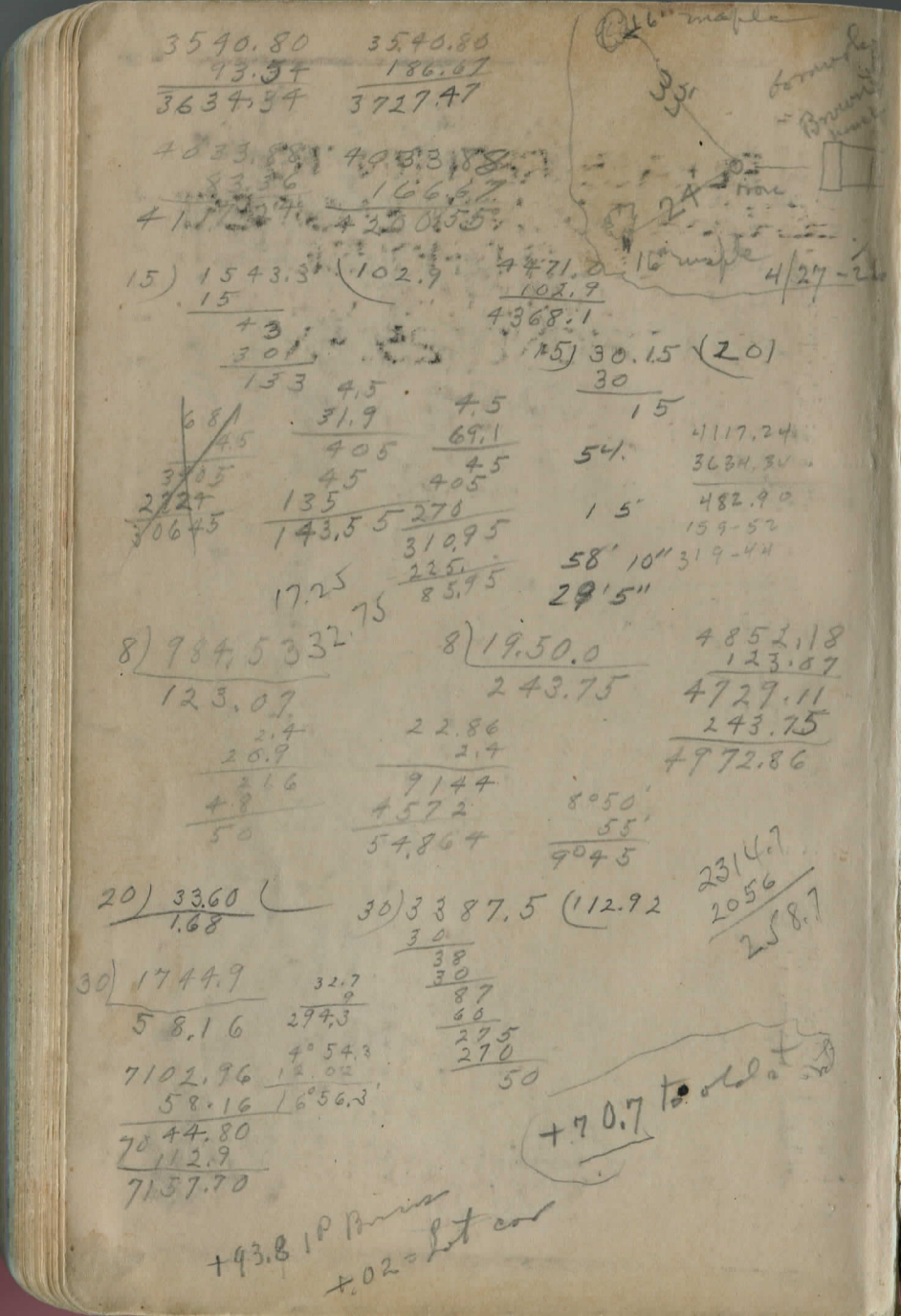
EXPLANATION AND USE OF TABLES

Stations.—Given P. I.=Sta. 161+60.35 to find Sta. of P. C. and P. T. Δ=62° 10′ D=8° 20′. From Table IV for 1° curve T=3454.1 and÷8⅓=414.49 ft. From Table V correction=.36 or T=414.85 ft. P. C.=Sta. P.I.—T=157+45.50. Also from (4) L=746.00 and P. T.=Sta. P. C.+L=164+91.50.

Offsets.—Tangent offsets vary (approximately) directly with D and with square of the distance. Thus tangent offset for Sta. 158 on above curve is 2.16 ft. found as follows. From Table III tangent offset for 100 ft.=7.27 ft. Distance=158—Sta. P. C.=54.50, hence offset=7.27 $(54.50\div100)^2$=2.16 ft. Also square of any distance divided by twice the radius equals (approximately) the distance from tangent to curve. Thus $(54.50)^2\div(2\times688.26)$=2.16 ft.

Deflections.—Deflection angle=½ D for 100 ft., ¼ D for 50 ft., etc. For c ft.=(in minutes) .3 x C x D° or=defl. for 1 ft. from Table III x C. For Sta. 158 of above curve=.3 x 54.5 x 8⅓=136.2′ or 2° 16.2′, or=2.50 x 54.5=136.2′ from Table III. For Sta. 159 deflection angle=2° 16.2′+8° 20′÷2=6° 26.2′, etc.

Externals.—May be found in similar manner to tangents. Thus E for curve above is 91.37. For from Table IV for 1° curve E=960.6 for 8° 20′=960.6÷8⅓=91.27 and from Table V correction=.10 or E=91.37 ft. Or suppose Δ=32° and E is measured and found to be 42 ft. What is D? From Table IV E=230.9 and÷42=5.5 or D=5° 30′.



DISTANCES FROM CENTER OF ROADWAY FOR CROSS-SECTIONING.

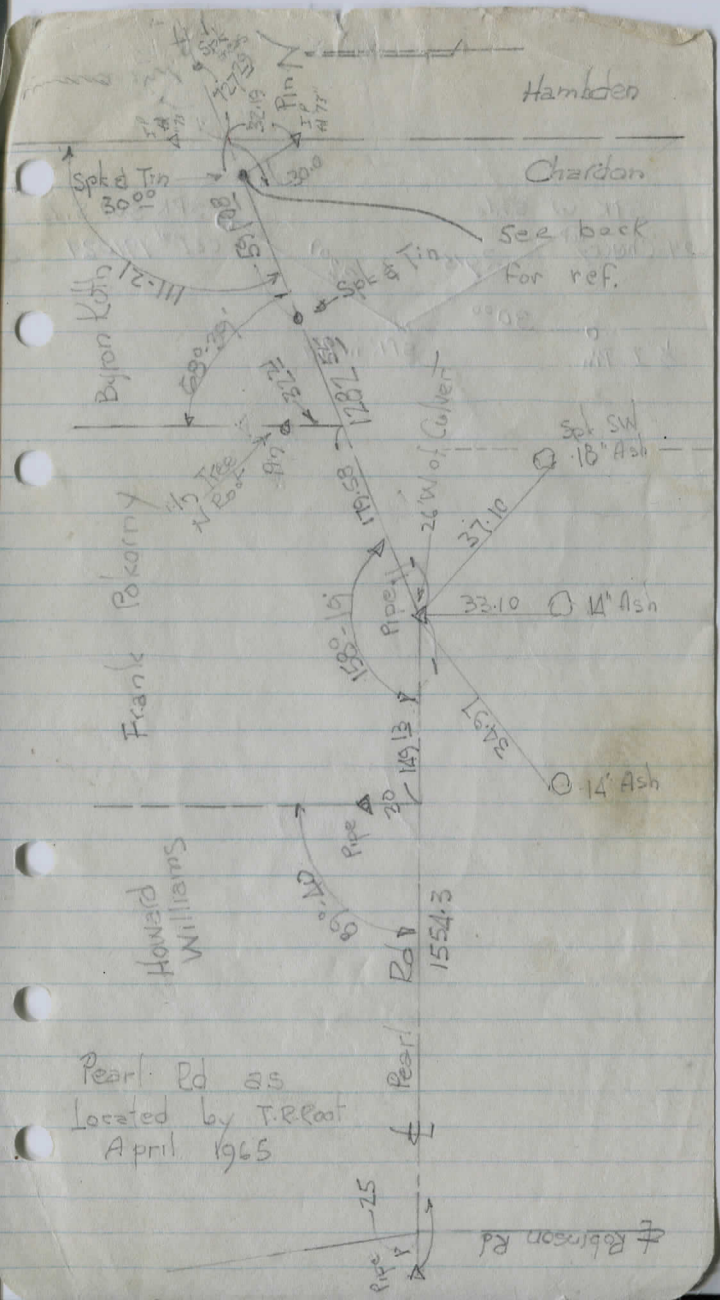
Roadway 18 feet wide. Side Slopes on 1:2.

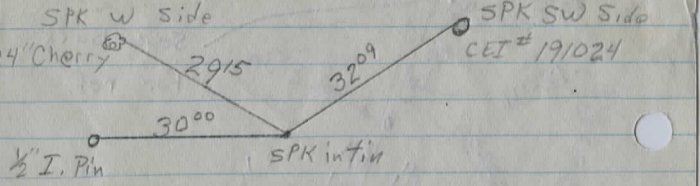
For Single Track Embankment.

H.	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	H
0	8.0	8.2	8.3	8.5	8.6	8.8	8.9	9.1	9.2	9.4	0
1	9.5	9.7	9.8	10.0	10.1	10.3	10.4	10.6	10.7	10.9	1
2	11.0	11.2	11.3	11.5	11.6	11.8	11.9	12.1	12.2	12.4	2
3	12.5	12.7	12.8	13.0	13.1	13.3	13.4	13.6	13.7	13.9	3
4	14.0	14.2	14.3	14.5	14.6	14.8	14.9	15.1	15.2	15.4	4
5	15.5	15.7	15.8	16.0	16.1	16.3	16.4	16.6	16.7	16.9	5
6	17.0	17.2	17.3	17.5	17.6	17.8	17.9	18.1	18.2	18.4	6
7	18.5	18.7	18.8	19.0	19.1	19.3	19.4	19.6	19.7	19.9	7
8	20.0	20.2	20.3	20.5	20.6	20.8	20.9	21.1	21.2	21.4	8
9	21.5	21.7	21.8	22.0	22.1	22.3	22.4	22.6	22.7	22.9	9
10	23.0	23.2	23.3	23.5	23.6	23.8	23.9	24.1	24.2	24.4	10
11	24.5	24.7	24.8	25.0	25.1	25.3	25.4	25.6	25.7	25.9	11
12	26.0	25.2	26.3	26.5	26.6	26.8	26.9	27.1	27.2	27.4	12
13	27.5	27.7	27.8	28.0	28.1	28.3	28.4	28.6	28.7	28.9	13
14	29.0	29.2	29.3	29.5	29.6	29.8	29.9	30.1	30.2	30.4	14
15	30.5	30.7	30.8	31.0	31.1	31.3	31.4	31.6	31.7	31.9	15
16	32.0	32.2	32.3	32.5	32.6	32.8	32.9	33.1	33.2	33.4	16
17	33.5	33.7	33.8	34.0	34.1	34.3	34.4	34.6	34.7	34.9	17
18	35.0	35.2	35.3	35.5	35.6	35.8	35.9	36.1	36.2	36.4	18
19	36.5	36.7	36.8	37.0	37.1	37.3	37.4	37.6	37.7	37.9	19
20	38.0	38.2	38.3	38.5	38.6	38.8	38.9	39.1	39.2	39.4	20
21	39.5	39.7	39.8	40.0	40.1	40.3	40.4	40.6	40.7	40.9	21
22	41.0	41.2	41.3	41.5	41.6	41.8	41.9	42.1	42.2	42.4	22
23	42.5	42.7	42.8	43.0	43.1	43.3	43.4	43.6	43.7	43.9	23
24	44.0	44.2	44.3	44.5	44.6	44.8	44.9	45.1	45.2	45.4	24
25	45.5	45.7	45.8	46.0	46.1	46.3	46.4	46.6	46.7	46.9	25
26	47.0	47.2	47.3	47.5	47.6	47.8	47.9	48.1	48.2	48.4	26
27	48.5	48.7	48.8	49.0	49.1	49.3	49.4	49.6	49.7	49.9	27
28	50.0	50.2	50.3	50.5	50.6	50.8	50.9	51.1	51.2	51.4	28
29	51.5	51.7	51.8	52.0	52.1	52.3	52.4	52.6	52.7	52.9	29
30	53.0	53.2	53.3	53.5	53.6	53.8	53.9	54.1	54.2	54.4	30
31	54.5	54.7	54.8	55.0	55.1	55.3	55.4	55.6	55.7	55.9	31
32	56.0	56.2	56.3	56.5	56.6	56.8	56.9	57.1	57.2	57.4	32
33	57.5	57.7	57.8	58.0	58.1	58.3	58.4	58.6	58.7	58.9	33
34	59.0	59.2	59.3	59.5	59.6	59.8	59.9	60.1	60.2	60.4	34
35	60.5	60.7	60.8	61.0	61.1	61.3	61.4	61.6	61.7	61.9	35
36	62.0	62.2	62.3	62.5	62.6	62.8	62.9	63.1	63.2	63.4	36
37	63.5	63.7	63.8	64.0	64.1	64.3	64.4	64.6	64.7	64.9	37
38	65.0	65.2	65.3	65.5	65.6	65.8	65.9	66.1	66.2	66.4	38
39	66.5	66.7	66.8	67.0	67.1	67.3	67.4	67.6	67.7	67.9	39
40	68.0	68.2	68.3	68.5	68.6	68.8	68.9	69.1	69.2	69.4	40

Example—If point is 22.6 ft. above grade, how far should it be from center line to be a slope stake point? Ans. from Table 41.9. For same slopes but other widths of roadbed correct above figures by one-half difference in width of roadbed; thus in example above for 20 ft. roadbed distance will be 41.9+(20—16)÷2 or 2 ft. added to 41.9 =43.9. For slopes of 1 on 1 see inside of front cover.

Made in Germany.


Hambden
Charlton
Spkd Tin
See back
for ref.
Spkd Tin
Byron Kuhn
Spkd SW
18" Ash
Pipe
26 W of Culvert
37.10
33.10
14" Ash
14" Ash
Pipe
Frank Pokorny
Howard Williams
Pipe
Pearl Rd
Pearl Rd as
Located by T.R.Peat
April 1965
Robinson Rd


SPK W Side
24" Cherry
29.15
30°00
½" I. Pin
SPK in Tin
32°09
SPK SW Side
CEI # 191024

Pg 4

Brown Rd. Re information.

N

I.P. fd & used Fd. 10.80

I.P. fd & used.

Woodin Rd.

90°

Rec. S 89° E 3371 008

30.67 10" NAIL SET

Rec. S 89° E 3371 014 Mea. 572191

29.01 10" NAIL SET

NEAR NEND 14.0" ASH B-2468

TRAILER CAMP

I.P. Set.

4983.71 EDM

4783.80

33.55 CALC. 80

148.15

148 15

I.P. Set.

702.28 Rec.

465.27

FD. 10.80

I.P. Set.

108° 15'

108 15 57.3 AOT.

±342' TO RIVER

Rec.

791.79'

791.84 EDM

139° 40' 17"

I.P. Set.

FD. 10.80

2418.56 Mea.

I.P. Set.

R.R. SPK Fd. 10.80

I.P. Set.

Pearl Rd.

Centerline Information
on Brown Rd. from
Woodin Rd. to Pearl Rd.
Feb. 1956.

Pg. 1

Pearl Rd.
E Intersection

℄ S.R. 608

I.P. Rd. Assumed

211+82.65
I.P. Rd. Assumed

123°-02'-45"
Rec. # obs.

℄ S.R. 608

Note: Intersection on Iron pins on S.R. 608 are from State Highway Dept. records

℄ Pearl Rd 60'

See pg 3 for ref

Iron spk set with Punch Mk.

℄ Brown Rd 6.0'

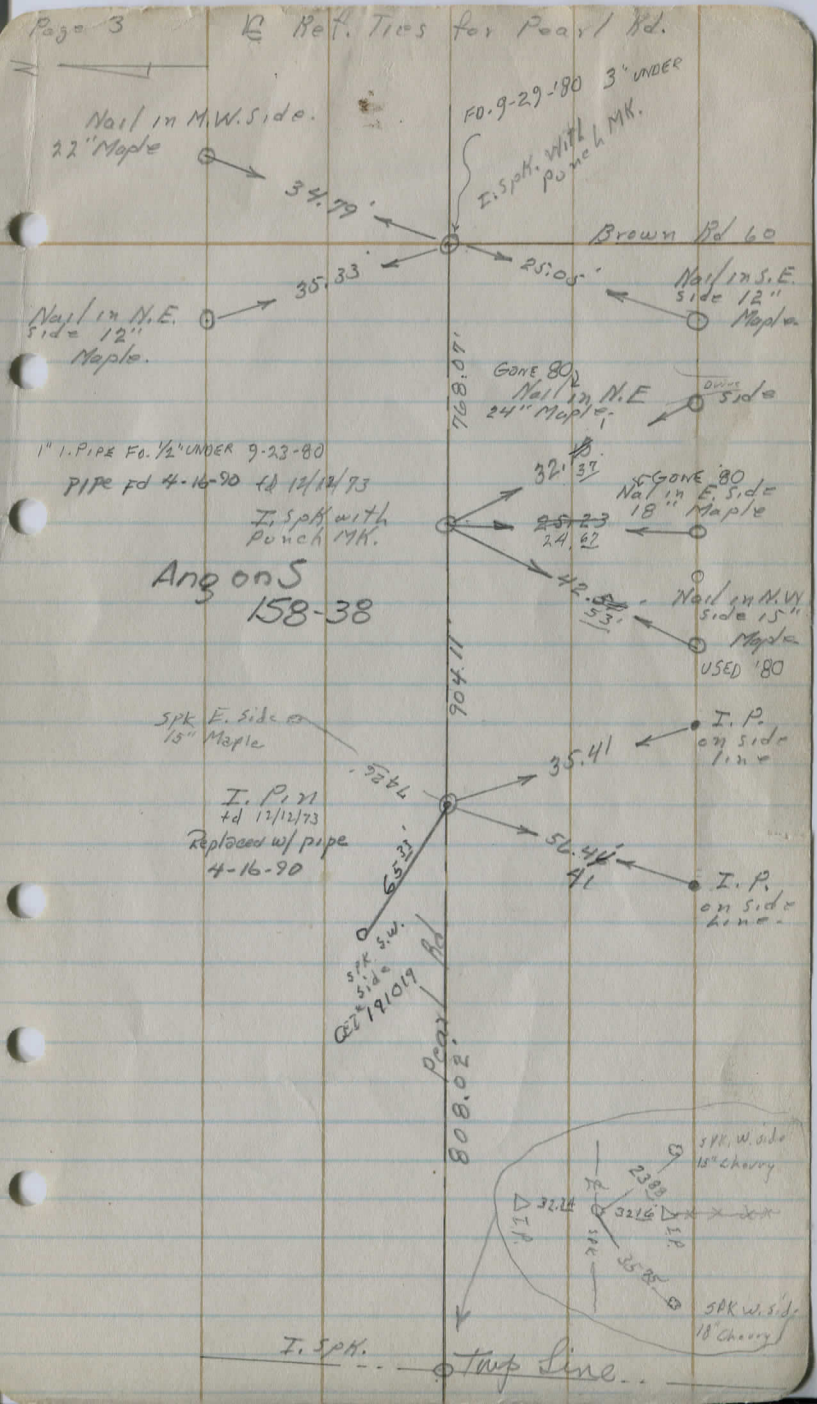
89°-44'-43"
obs.

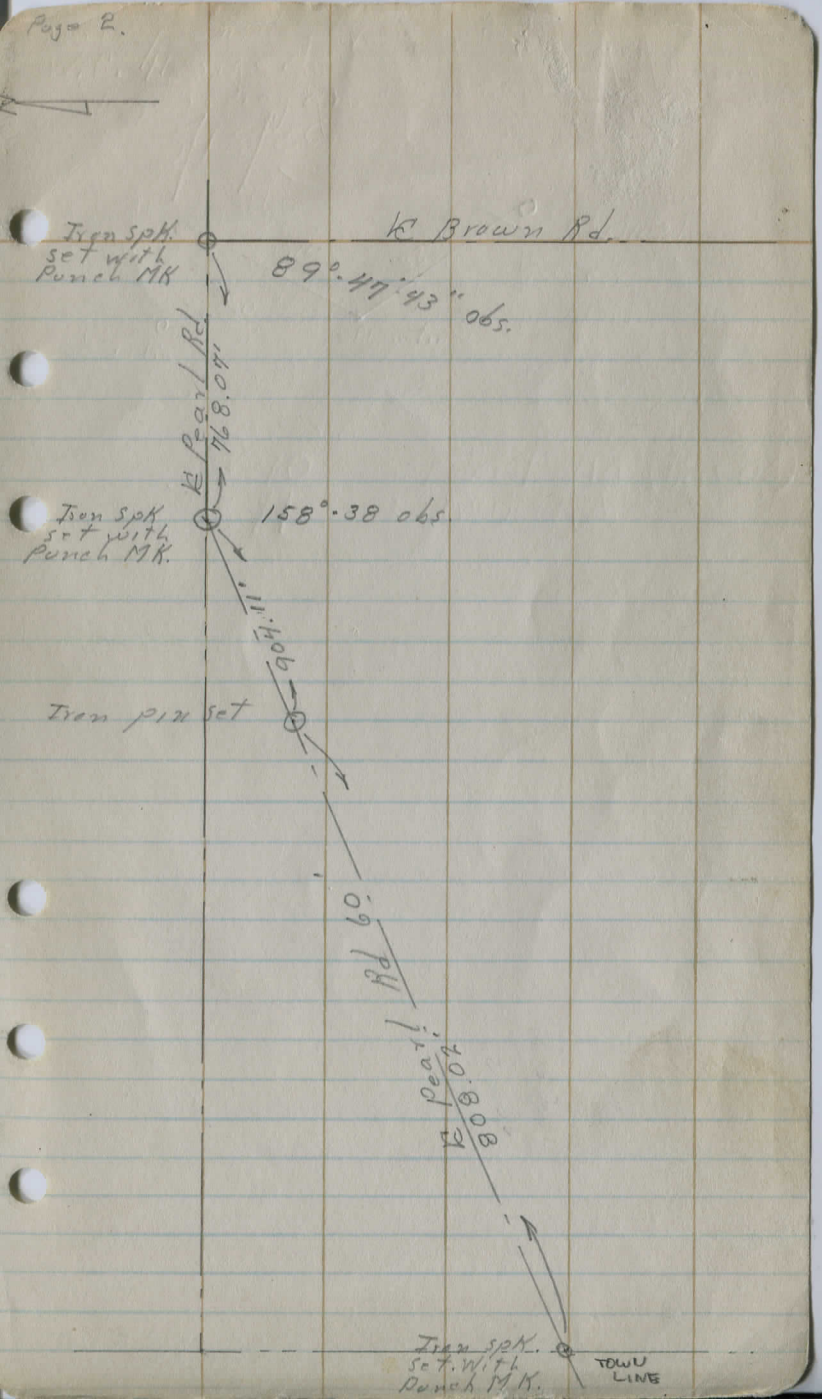
Survey made by
W.C. Hunger
Reg. Surveyor
8/18/56

Centerline Information
on Pearl Rd. from S.R. 608
West to Hambden Twp. line.
Feb. 1956

#70 Pearl Rd (E. end)
#71 Brown Rd.

℄ Ref. Ties for Pear / Rd.




Iron spk set with Punch MK
E Brown Rd.
89°-47'-43" obs.
E Pearl Rd.
N 8.0 ft.
Iron spk set with Punch MK.
158°-38 obs.
N 66° 11' E 1106.11 ft.
Iron pin set
S 69° 11' E 1210.88 ft.
Iron spk. set with Punch MK.
TOWN LINE